196

C

PROPERTY OF
KING COUNTY
ENGINEER'S OFFICE
905 COUNTY-CITY BLDG.
SEATTLE

PROPERTY OF
KING COUNTY
ENGINEER'S OFFICE
905 COUNTY-CITY BLDG.
SEATTLE

AUG 18 1988 MICRO

FIELD BOOK REGISTER

No. 196 6

Name	Taken Out	Returned

196 C

196-C

—INDEX—

Survey of Elk Corral

	Pages
M^3 West Line Corral	65-66
East Margin Auburn Park Boulevard bet. Sta. 50+64 $\frac{73}{D}$ and sta. 56+95 $\frac{2}{}$	67
C^3 Line East fence Line of Corral along top of Bluff	68
N^3 Line Revised fence Line of Corral on W. + S. sides	61
H^3 Line Revised fence Line on the E. + S. sides	62
Portion of Meanders of Rt. Bank of White R. in Sec. 29-21-5	63
Sketch Sec. 29-21-5	69
Transcript Govt. Field notes Sec. 29-21-5	70-71

INDEX

00

Stuck River Survey

		Page
A^3 Line	Transit	1 - 6
	Levels	27 - 31
c^3 Line	Transit + Levels	7
J^3 Line	Transit	8
	Levels	37 - 38
B^3 Line	Transit	11 - 16
	Levels	33 - 36
D^3 Line	Transit	19 - 20
	Levels	59 - 60
d^3 Line	Transit	9
	Levels	39
e^3 Line	Transit	10
	Levels	40
I^3 Line	Transit + Levels	17
F^3 Line	Transit	21-24
	Levels	53-56
K^3 Line	Transit	25
	Levels	26
a^3 Line	Transit	64
	Levels	32
f^3 Line	Transit	42
	Levels Book 196 E P.	42 - 43
g^3 Line	Transit	43
	Levels B. 196 E P.	44-45
h^3 Line	Transit	44-43
	Levels B. 196 E. P.	46-48
i^3 Line	Transit	46
	Levels B. 196 B. P.	37-38
j^3 Line	Transit	41
	Levels B. 196 E. Page	41
k^3 Line	Transit	47
	Levels B 196 B P.	39
l^3 Line	Transit	48
	Levels B. 196 B. P.	40
m^3 Line	Transit	49
	Levels B196B P.	41
n^3 Line	Transit	50
	Levels B196B P.	42
o^3 Line	Transit	51
	Levels B 196 B P.	43
p^3 Line	Transit	52
	Levels B. 196 B. P.	44

Rainfall

From	To	Remarks
4:30 P.M. 1/23/13	7:00 A.M. 1/24/13	5/8"
7:00 A.M. 1/24/13		

2/19/13
2/20/13
2/21/13

READINGS ON GAGUE SET in River
100 S. of Sta. 3+90 $\frac{0}{0}$ A³ Line so that Elevations on gague correspond to other elevation taken for levels and topography above datum for Auburn Park Survey

1/23/13 Sherman

Reading	Date.	Hour.	Remarks		
94.0	1/3/13	8:A.M.	Highest water.		
89.0	1/24/13	2: P.M.	River rising Heavy rainfall. snow going off		
90.2	"	5:30 P.M.	" "	"	"
91.6	1/25/13	7: A.M.	Fair warmer		
92.1	1/25/13	6:30 P.M.	warm snow gone		
91.7	1/26/13	9:15 A.M.	Foggy cooler		
91.5	"	1:45 P.M.	Clear warm		
91.1	"	3:30 "	Cooler Foggy		
90.6	1/27/13	8:00 A.M.	Foggy Cold		
90.6	"	12: M.	very Foggy cool Spinkles		
90.4	1/28/13	2: P.M.	Cold Foggy		
90.5	"	5: "			
90.2	1/29/13	8: A.M.	Foggy	Temp.	40°
90.1	"	6: P.M.	"	"	50°
90.2	1/30/13	8: A.M.	Clear	"	45°
90.2	"	5: P.M.	Clear	"	50°
90.1	1/31/13	8: A.M.	Foggy mist	"	50°
90.0	"	5: A.M.		"	45°
90.0	2/1/13	8: A.M.	Clear cool	"	40°
89.9	"	5: P.M.	" "		
89.9	2/2/13	8: A.M.	" "	"	32°
89.9	"	5: P.M.	" "	"	42°
90.0	2/3/13	8: A.M.			
90.1	"	12: M.			
90.3	"	5: P.M.	Rain.		45°
90.3	2/4/13	8: A.M.	Snow		
90.3	"	5: P.M.	Snow		40°
90.1	2/5/13	7: A.M.			31°
90.0	"	5: P.M.		8 P.M.	35°
89.9	2/6/13	8: A.M.			
"	"	5: P.M.			
89.8	2/7/13	8: A.M.			
"	"	5: P.M.			
89.6	2/8/13	8: A.M.			28°
89.5	"	5: P.M.		9: P.M.	33°
89.5	2/9/13				
89.5	2/10/13				
89.4	2/11/13				
89.4	2/12/13	8: P.M.			
89.2	2/13/13				
89.8	2/14/13				
90.8	2/15/13	6: P.M.			
Same 90.9	2/16/13				
91.4	2/17/13	8: A.M.			
91.2	2/18/13	8: A.M.			
91	"	5: P.M.			

Survey for the Location of the White and Stuck Rivers up stream from Auburn Park to the uppermost point of seperation.

A^3 Line Up Along the Left Bank Present River

Angle C. Course M. Course

970.29

(2) 9+30 20 △ 69-46-30 Lt N. 22°-14'-00" E N 22°-15' E

539.74

(1) 3+90 46 ⊙ Hub ℄ Brush concrete Bulkhead

390.46

Set Compass with a variation set off that would give meat true brg. of lines corresponding to the meridian used for the Survey of Sec. 29-21-5.

17+00 "A" Line
=0+00 △ 0°-33'-15" Rt. S87°-57'-30" E S88° E
B.S. on 8+00
"A" Line Vol. 196 A P.2

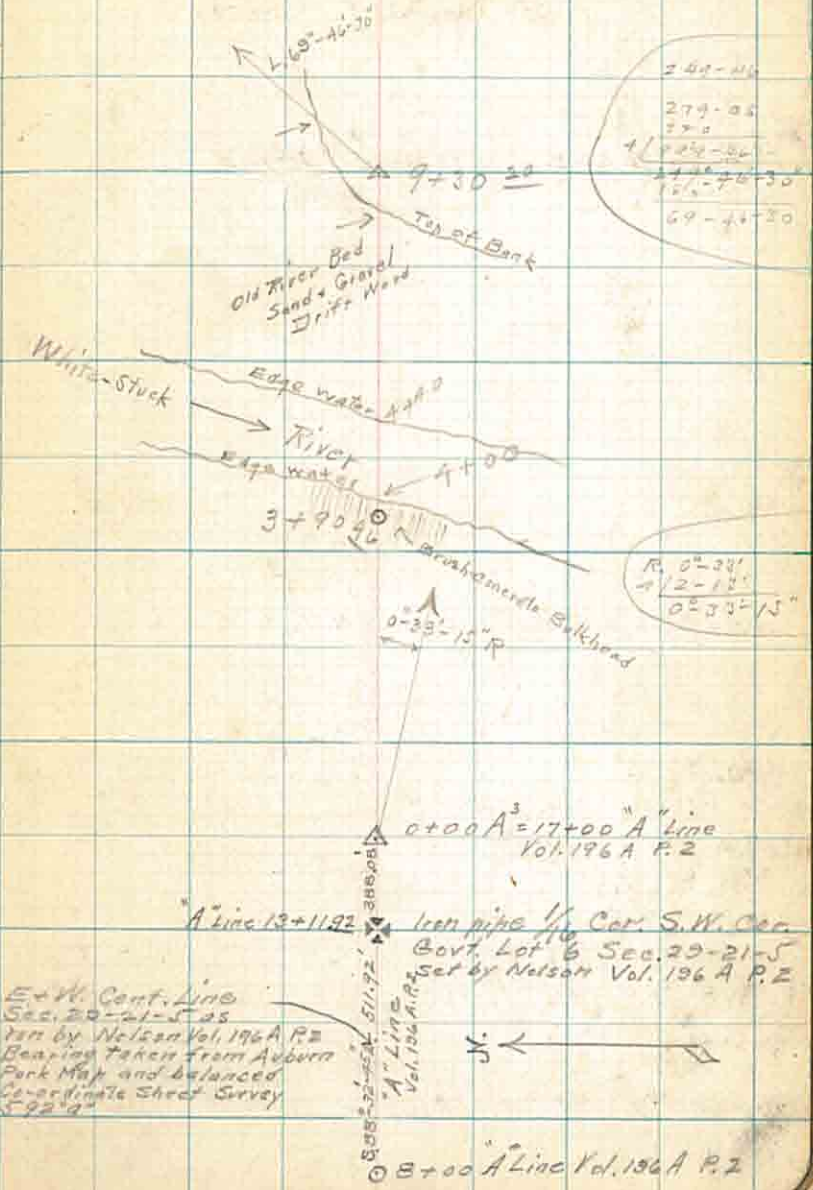
For a starting point I took a hub 17+00 on the "A" Line Vol. 196 A P.2. Before accepting this point as correct I checked the A Line both for measurement and alignmet from the Iron pipe 1/4 cor. Bet. 29-30 S.88°-32'-48" E. along the E.+W. Cent. Line of Sec. 29-21-5 to Sta. 17+00 and found it to be correct within a reasonable error.

Clyde W. Sherman

Began Dec. 21, 1912

1

(Deputy) Clyde W. Sherman
J. H. York
W. H. Hart
J. F. Keener



A³ Line Up Along the Left Bank Present River

Dec. 23, 1912.

Sherman
York
Hart
Keener

2

1 error.
379.68
~~378.68~~

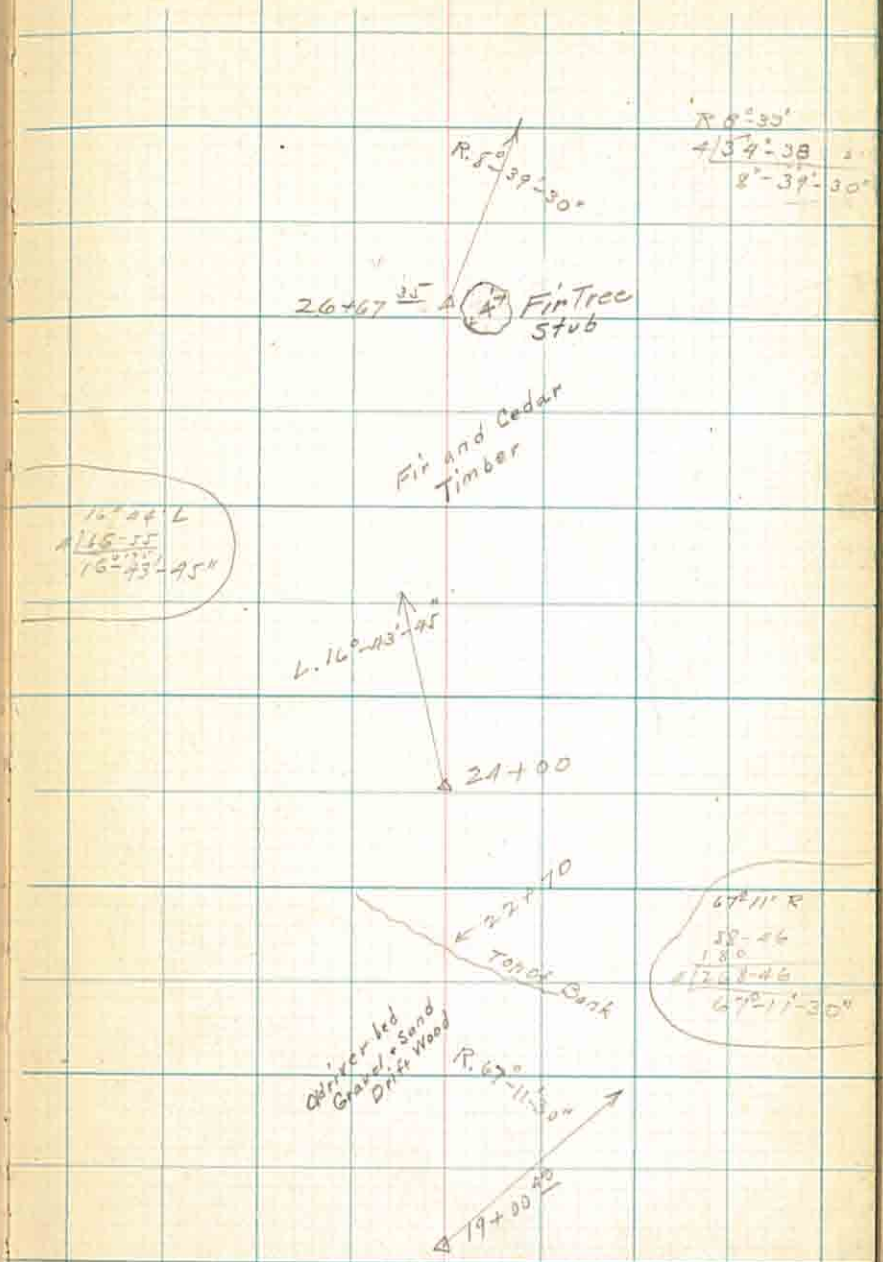
③ 26+67 35 △ R.8°-39'-30" N.81-21-15 E N.81°30' E.

267.35

④ 24+00 △ L16°-43'-45" N72°-41'-45" E N.72°50' E.

499.51

③ 19+00 49 △ 67°-11'-30" Rt. N89°-25'-30" E N.89°40' E.



A³ Line Up Left bank Present River

643.08

(1) 47+33 80 △ R. 74°-23'-00 S 14°-27'-30" E S. 19°-30' E

456.35

(2) 42+77 45 △ R. 36°-25'-30" N 86°-09'-30" E N. 86°-15' E

417.45

(3) 38+60 ⊙ on line

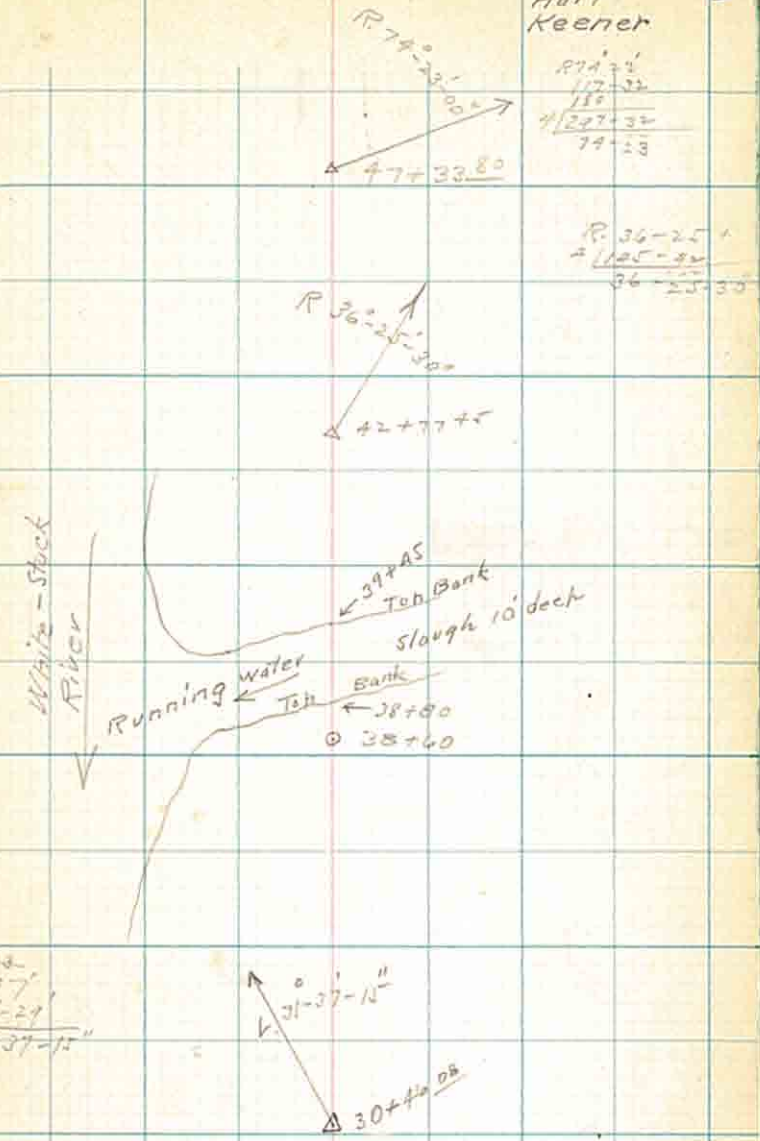
813.97

(4) 30+46 08 △ L. 31°-37'-15" N 49°-44'-00" E N 49°45' E

Dec. 24, 1912.

Sherman
York
Hart
Keener

3



A³ Line Up Left Bank Present River

620.10

(12) 71+74.60 △ R.51°-03'-15" S.30°-02'-15" E S.30°-15' E.

1258.35

(11) 59+16.25 △ L 27°-42'-00" S. 81°-05'-30" E S 80°-45' E

539.37

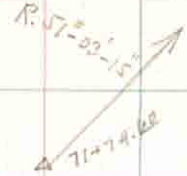
(10) 53+76.88 △ L 33°-56'-00" S 53°-23'-30" E S 53°-30' E

Dec. 26, 1912

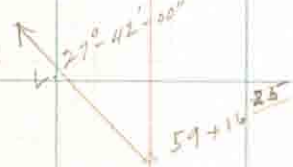
Sherman
York
Hart
Keener

4

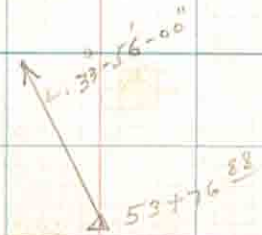
231-03
R. 51°-03
4 | 204-13
51°-03'-15"



L 207°-42'
27-42
4 | 110-48
27-42



213-56
4 | 135-44
L 33-56



A³ Line Up Left Bank Present River

(13) 93+00 △ R. 10°-47'-15" S. 65°-45'-00" E. S 65°-45' E.

1188.55'

(14) 81+11 45 △ L. 57°-57'-00" S. 76°-32'-15" E. S 76°-15' E

316.75

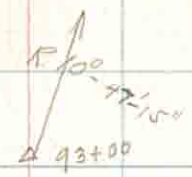
(15) 77+94 70 △ R. 11°-27'-00" S 18°-35'-15" E S 18°-30' E.

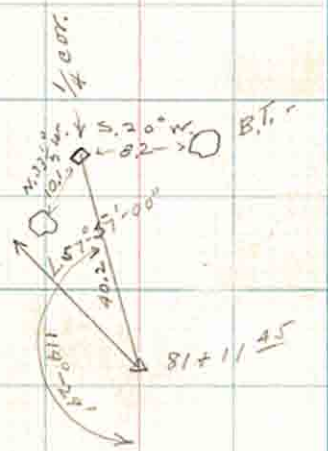
Dec. 27, 1912.

Sherman
York
Hort
Keener

5

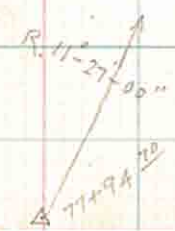
190-47
R. 10-47
4 | 43-09
10°-27'-15"





237-57
1 L 57-57
4 | 231-48
57-57

191-27
R. 11-27
4 | 45-48
11°-27'



A³ Line Up. Left Bank Present River

12/27/12

Sherman
York
Hart
Keener

6

101+65 92 △ end

△ 101+65 92

865.92

(15)

93+00 △

S.65°-45'-00"E

△ 93+00

O^3 Line

Transit + Levels

	Rod	H. I.	Elev.
B.M.	+1.14	100.82	99.68
0+00 ○/△	5.96		94.86
1	6.4		94.4
2	4.9		95.9
3	6.2		94.6
4	8.7		92.1
5	7.9		92.1

5+00 end

0+00 △
= 6+09 ○
A^3 Line

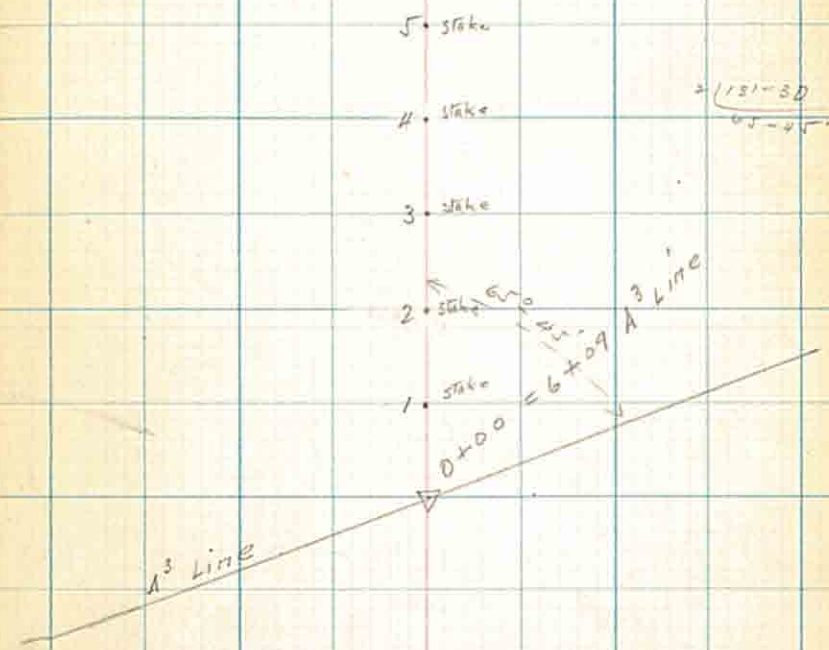
N. 26°-20' E

1/31/13

Sherman Hart

7

Rig foot bank 8+90 A^3 line P. 27
on hub



J³ Line Transit

Levels on pages 37-38

25+83 1/Δ end

16+93 6/Δ R. 39°-08' S. 77°-55'-30" W, S. 77° W.

14+16 1/⊙

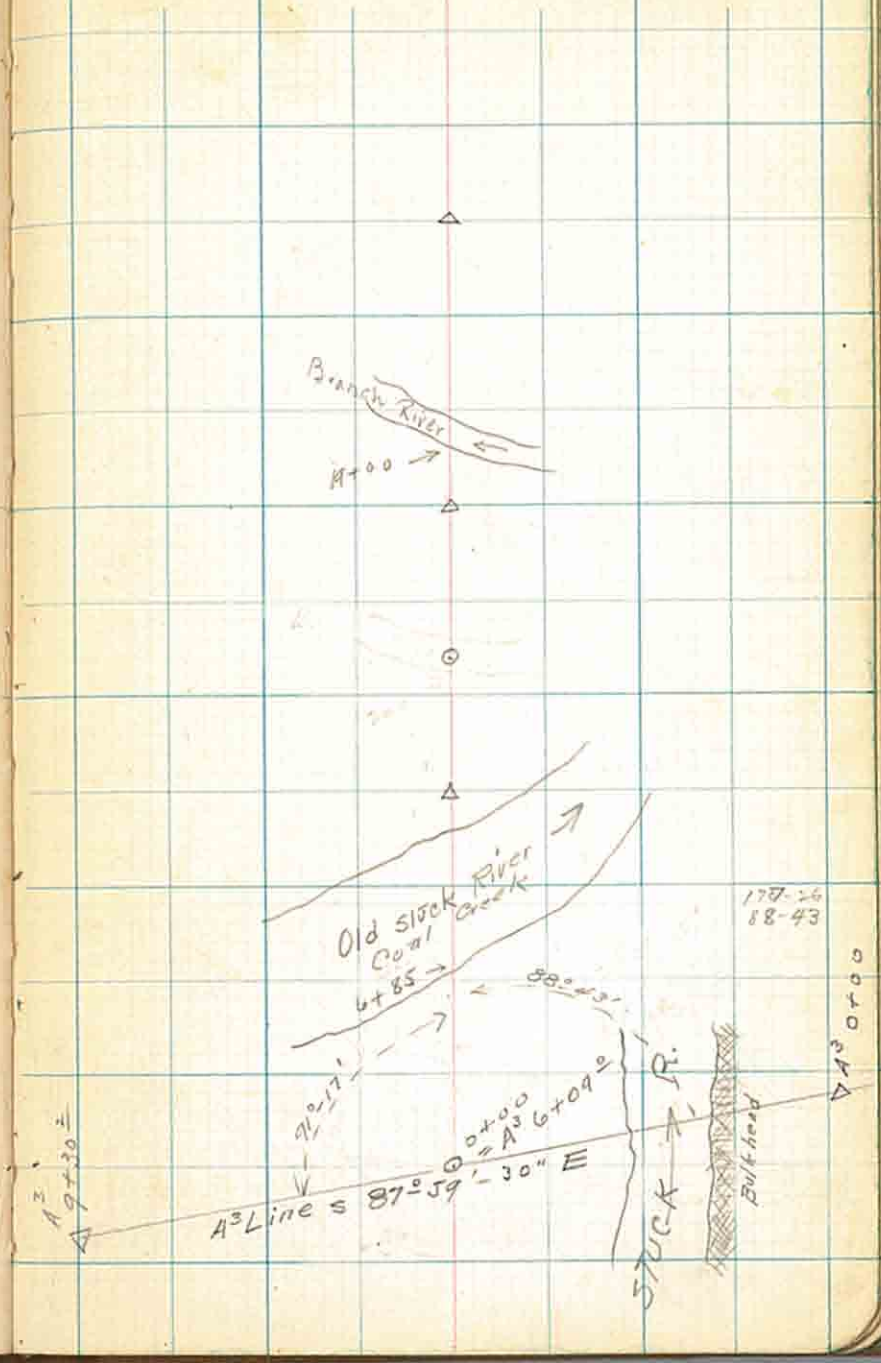
9+38 2/Δ R. 35°-30' S. 38°-47'-30" W, S. 37° W

0+00 ⊙ S. 3°-17'-30" E, S. 3°-30' W.

2/4/13 Snowing

Sherman
Bluher
Hartman
Keener

8



d^3 Line

Transit

Levels on page 39

7+00 end

1 +33 $\frac{3}{\odot}$ N. North

0+00 $\frac{1}{\odot}$ N. North

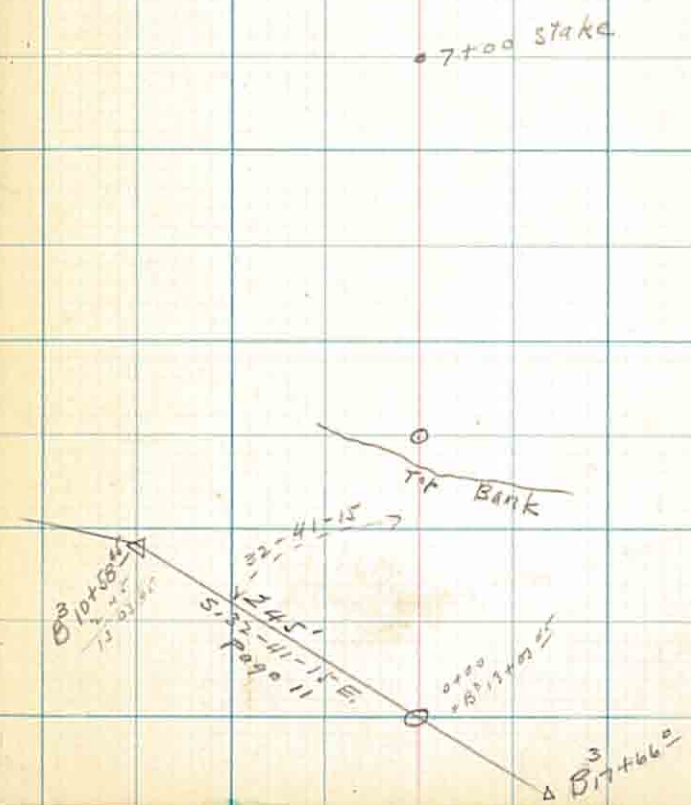
$= B^3$ 13+03 $\frac{45}{\odot}$

P. 11

2/4/13

Sherman
Bluher
Hart
Keener

9



e³

Transit

Levels on page 40

15+

15+00 end

7+99 4/⊙

5+87 3/⊙

3+10 5/⊙

0+00

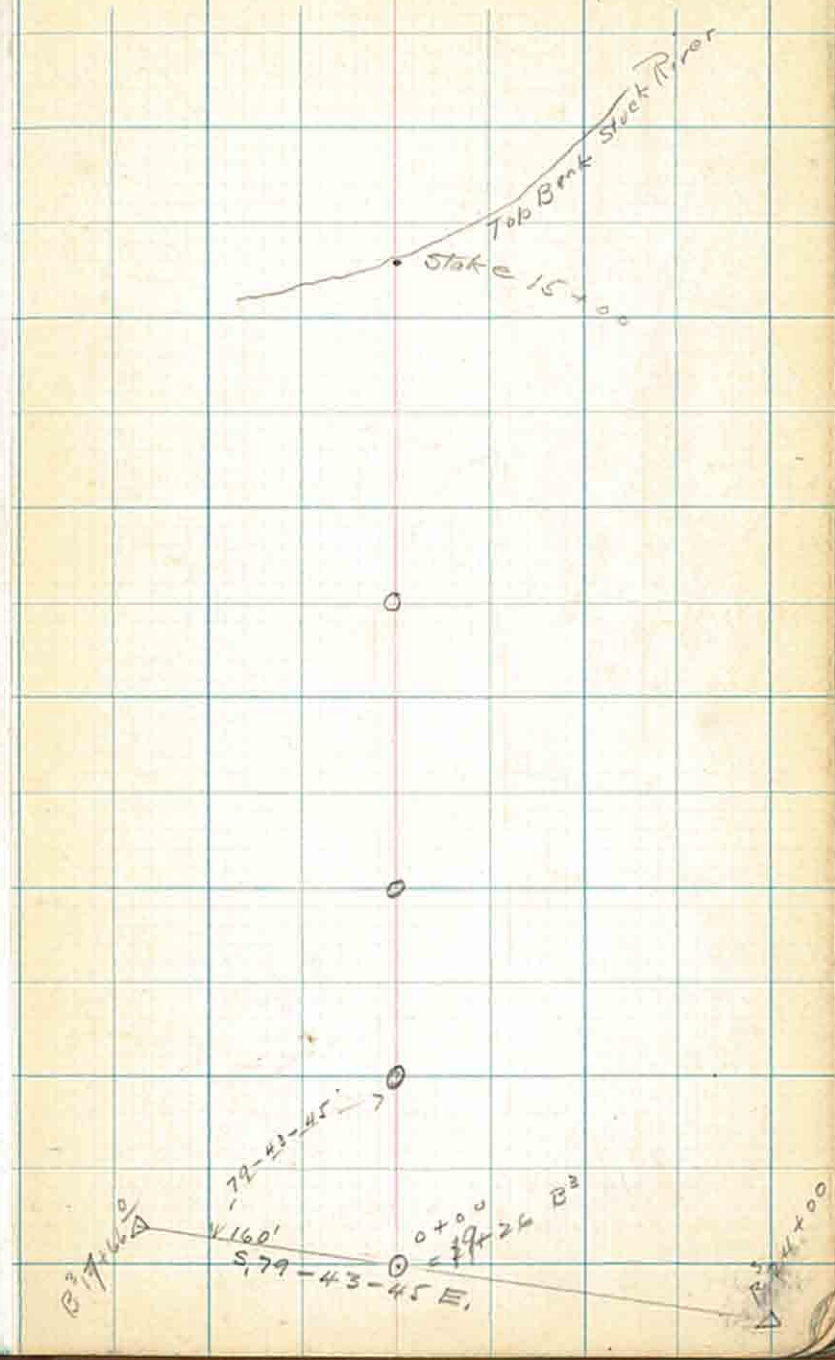
B³ 2/+26 0/0

P. 12

2/4/13

Snowing all day

Sherman
Bloher
Hart
Kaener



B^3 Line Up the old Stuck Channel

707.33

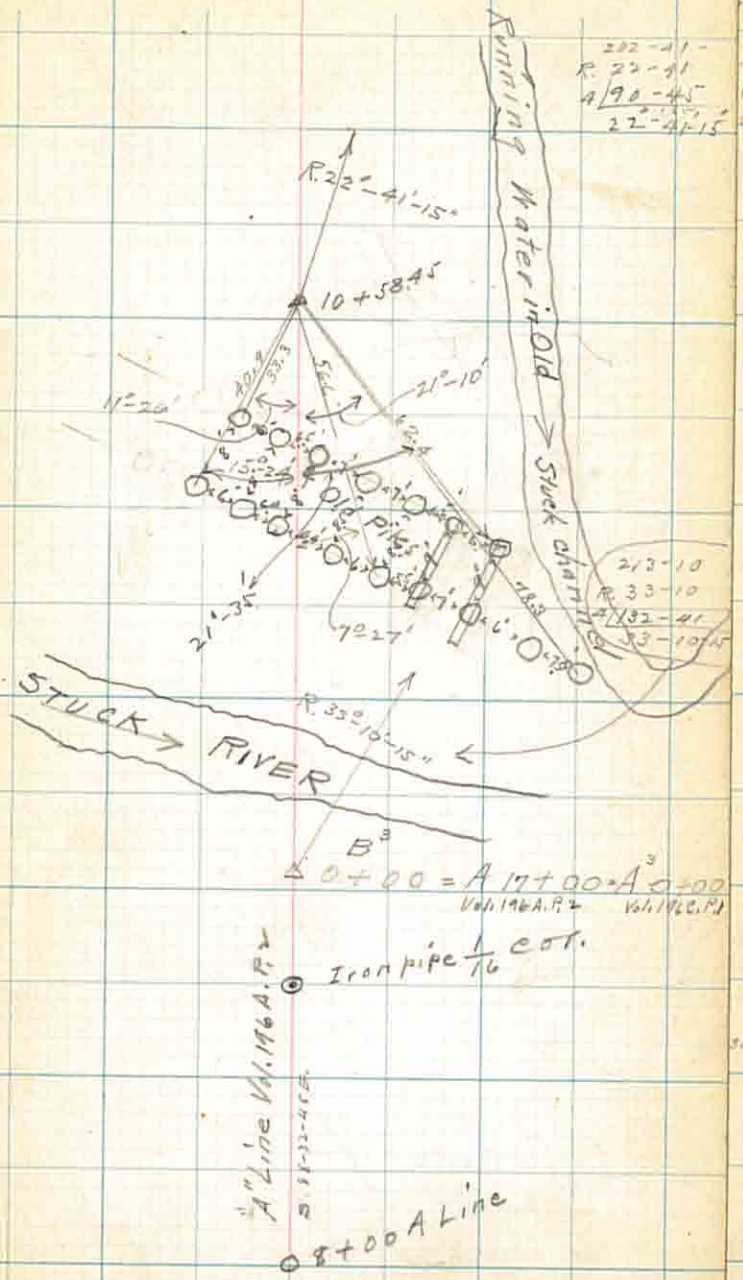
① 10+58.45 △ R. 22°-41'-15" S. 32°-41'-15" E S 33° E

1048.45
1058.45

0+00 △ R. 33-10-15 S. 55°-22'-30" E S. 55° E
=17+00
"A" Line.
Vol. 196 A.P. 2
B.S. on
8+00 "A" Line

Dec. 28, 1912.

Sherman
York
Hart
Keener



B³ Line Up Old Stock channel

946.50

29+00 00 △ R. 26°-52'-15" N.72°-29'-15" E. N.72°-30' E

500.00

24+00 00 △ L.54°-39'-15" N.45-37-00 E N 45° E

634.00

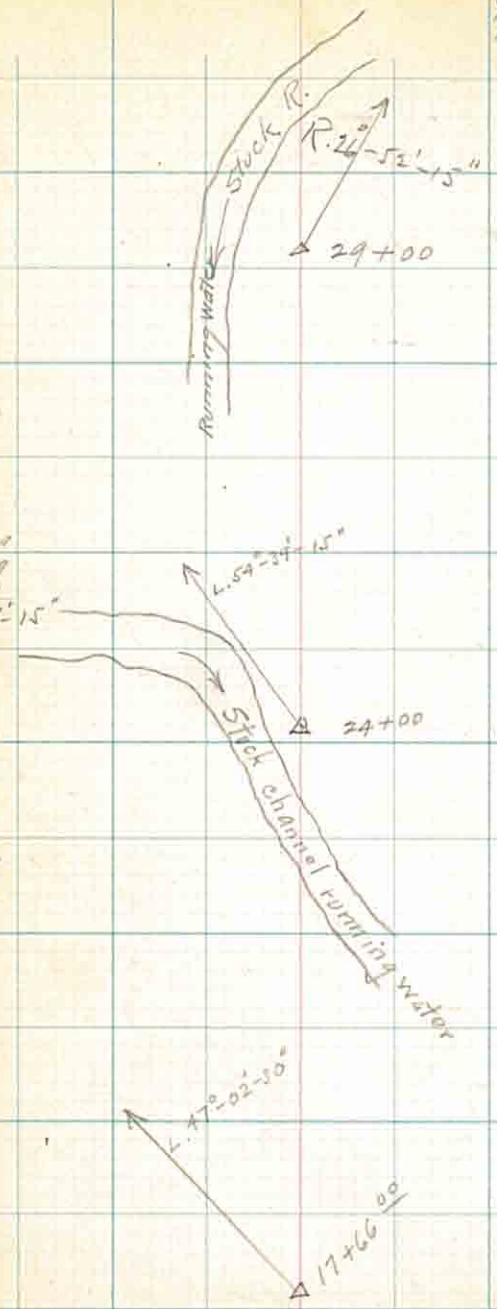
17+66 00 L. 47-02-30 S.79°-42'-45" E S 79° E

13/28/17

Sherman
Hart
York
Keener

12/2

R. 26°-52'
4 | 107-29
26°-52-15

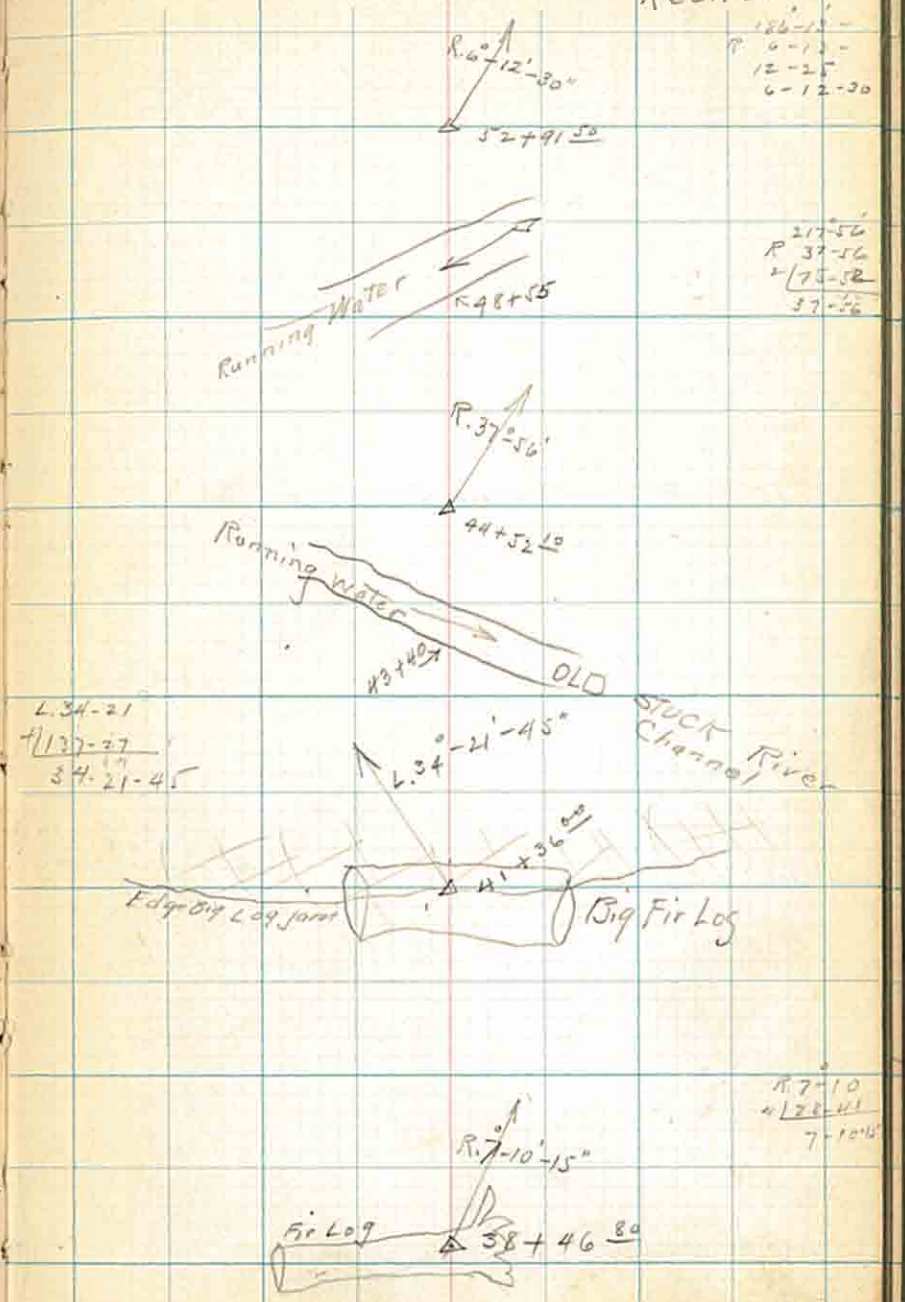


B³ Line Up old Stuck R. channel

1/2/13

Sherman
Bluher
Hart
Keener

	362.90			
(8) 52+91 50	Δ	R. 6-12-30	N. 89-26-15 E	N. 88°-30' E
	839.40			
(7) 44+52 10		R. 37°-56'	N. 83-13-45 E	N. 82°-30' E.
	316.10			
(6) 41+36 00		Δ L. 34-21-45	N. 45-17-45 E	N. 45-30 E
	289.20			
(5) 38+46 80		Δ R. 7°-10'-15"	N. 79-39-30 E	N. 79-30 E



B³ Line

Transit

424.3

(14) 71+35 7/△ R.30°-28'-30" S.4°-07'-45" W S. 4° W

508.2

(11) 66+27 50/△ R.57°-01' S.26°-12'-45" E S. 26°-30' E

562.70

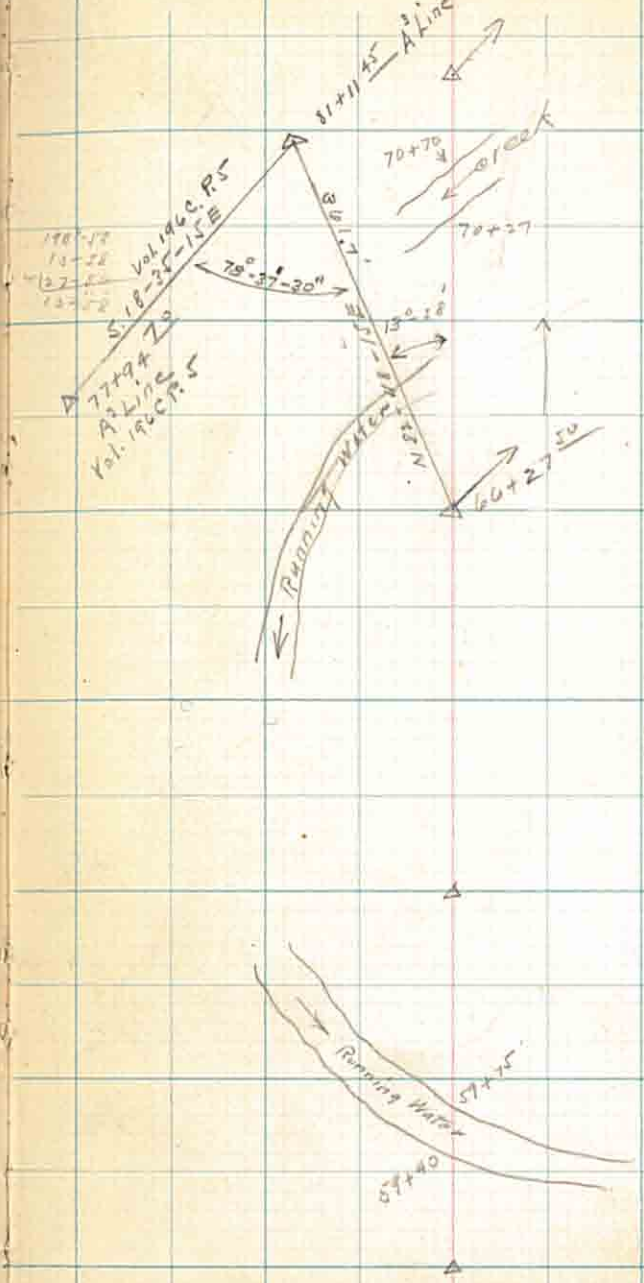
(10) 60+94 80/△ R. 31°-18'-30" S.83-13-45 E S 83° E

440.40

(9) 56+54 40/△ L.23°-58'-30" N 65°-27'-45" E N 65°-30' E

1/8/13

Sherman
Bluher
Keener



78-37
314-31
78°-37'-30"

S. 83-13-45 E
13-58
97-11-45
S. 32-48-15 E
W.
78-37-30
141-25-45
N. 18-34-15 W

B³ Line Transit

(14) 90 + 94 ³/₂ L. 35°-54' N. 41°-30'-15" E. N. 42° E. 491.9 215-54 71-48 35-54

358.7

(15) 87 + 35 ⁶/₂ L. 19°-26' N. 77°-24'-15" E. N. 78° E. 199-26 38-52 19-26

528.2

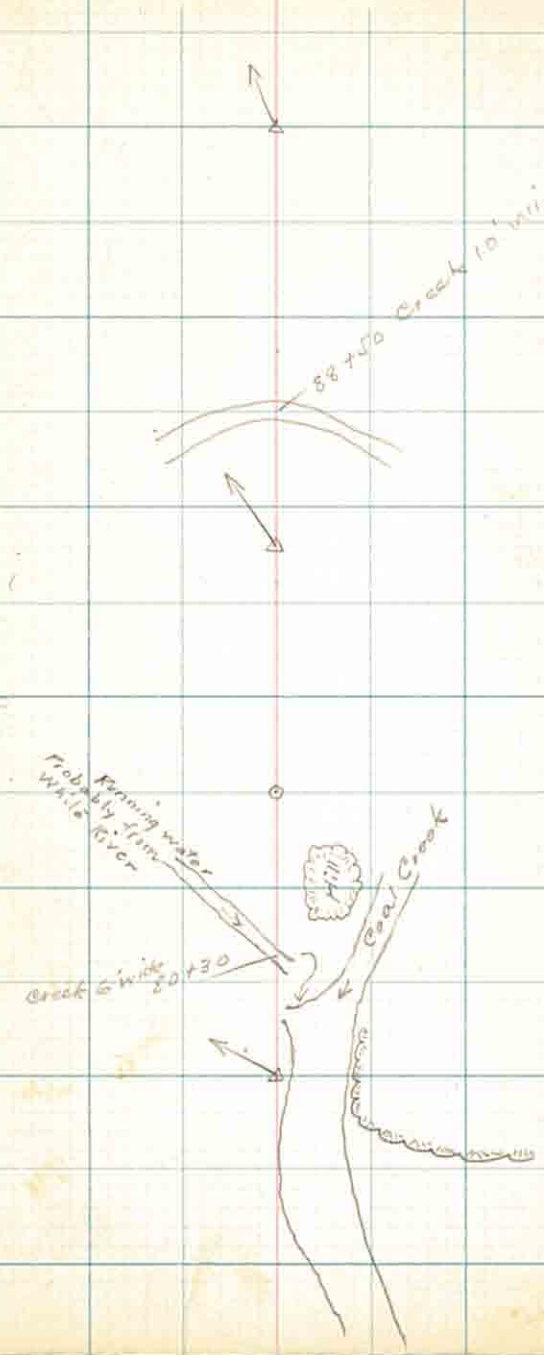
(16) 82 + 07 ⁴/₂ ⊙ on line S. 82°-30' E.

647.4

(13) 75 + 60 ⁰/₂ L. 87°-17'-30" S. 83°-09'-45" E. S. 82°-30' E. 267-17 174-25 87-17-30

1/29/13

Sherman Hart



B³ Line Transit

(18)
98+53 1/△ end
= A³ 101+

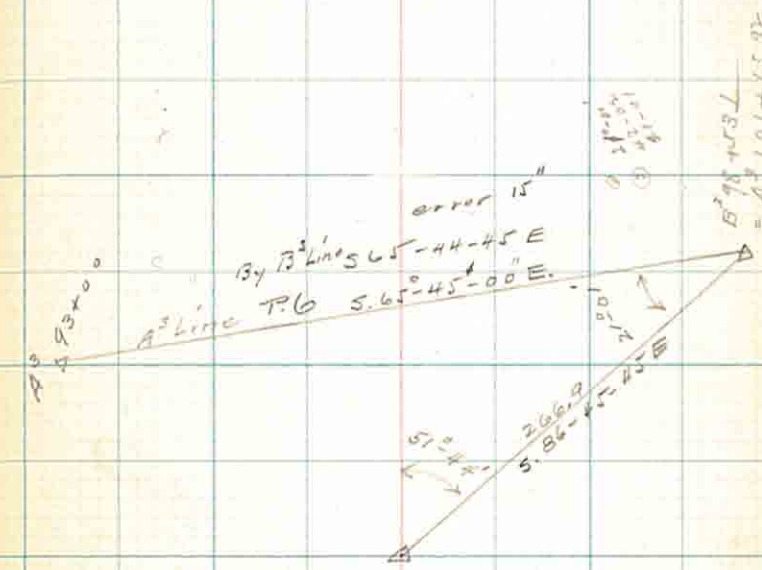
266.9

(17)
95+86 2/△ R. 51°-44' S.86°-45'-45" E S. 86°-20' E.

221'-44'
103-24
51-44'

1/29/13

Sherman Hart 106

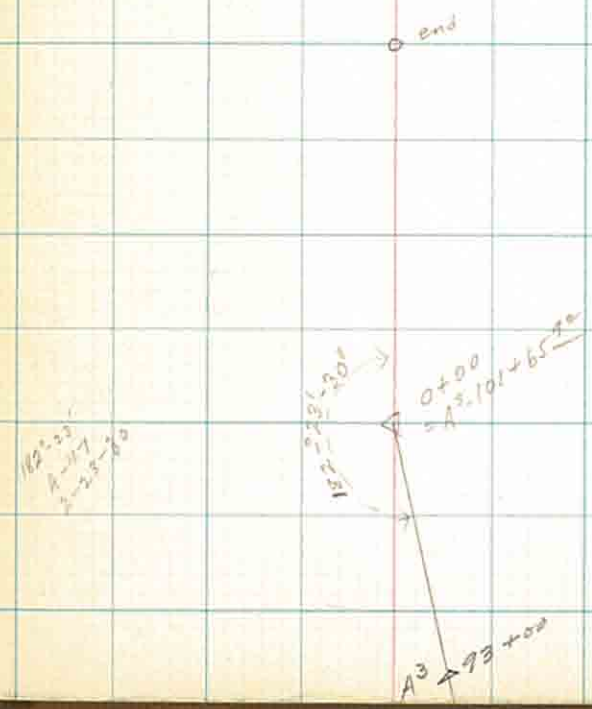


266.9
95 86.2
9853.1

I^3 Line — Transit + Levels

		Levels	
B. M.	+ 4.06	154.06	150.00
1+00	8.9		145.2
2	8.9		145.2
3	8.7		145.4
4	8.6		145.5
5	6.2		147.9
6	1.7		152.4
+28 $\frac{a}{\Delta}$	− 1.65		152.31
6+28 $\frac{a}{B}$	and		
0+00 $\frac{a}{\Delta}$			

Hub 101+65.92 A^3 Line Elev 150.0



D³ Line N. Side of Present River at Joe Bobs Ranch

Levels on Page 59

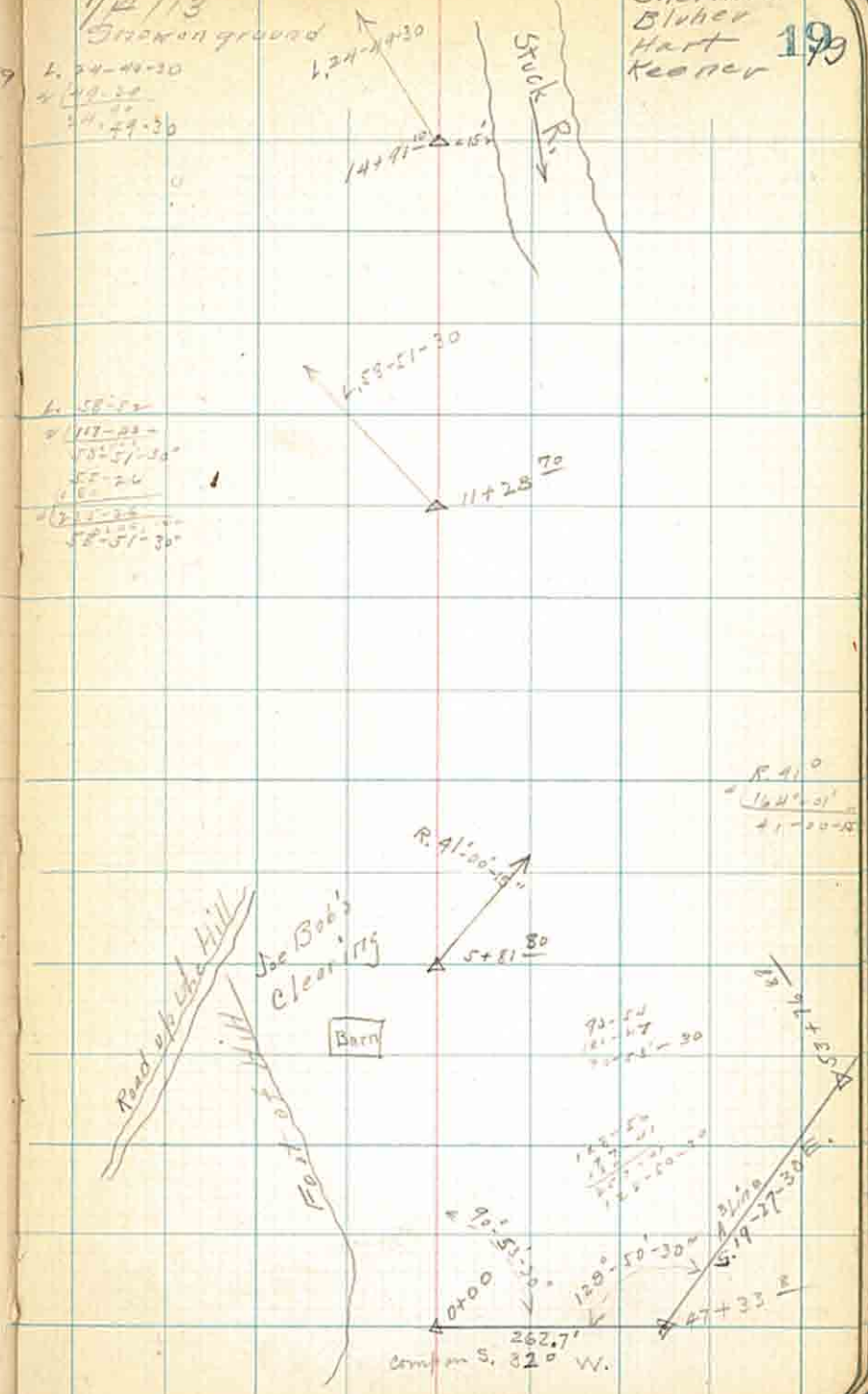
14+91.10 △		N. 78½° E
11+28.70 △		S 77° E
5+81.8		S. 18° E
0+00 △		S. 59¼° E.

1/12/13

Snow on ground

Sherman
Bluher
Hart
Keener

19



□ 3 Line

N. side Present River
at Joe Bobs old ranch

21+69 60 △

19+68 60 △

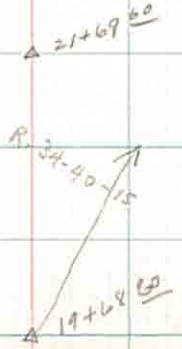
S 67° E

1/4/13

Sherman
Bluher
Hart
Keener

R. 84°-31
169°
84-30

△ 21+69 60



R. 34-40-15

R. 34-40-15

19+68 60

F³ Line Location Big Slide N. of Pt of Seperation Present + old stock River

88.10

③ 8+22 80 △ L 48° 57' S 67° 14' 15" E S. 67° 30' E

261.70

② 5+61 10 △ R. 16° 46' S 18° 17' 15" E S 18° 45' E

276.70

① 2+84 40 △ R. 39° 39' 30" S 35° 03' 15" E S. 35° E.

284.40

0+00 △ S 74° 42' 45" E S 75° E

1/5/13
Snow on ground

Sherman
Bluher
Keener

L. 48° 57'
97-54
48-57

L. 48° 57'

8+22 8

R. 16-46
33-32
16-46

R. 16° 46'

5+61 10

R. 39° 39' 30"

2+84 40

39-39
79-19
39-39-30
158-38
39-39-30

Top of Slide and Bluff

0+00

For connection with B³ Line see end of line Page 24

A³ hub 81+11 45 △

F^3 Line Location Big Slide

(8) 13+96 $\frac{54}{\Delta}$ R. 62°-38' N 4°-02'-15" W N. 4°-30' W.
12

142.06

(7) 12+54 $\frac{48}{\Delta}$ L. 2°-53'-30" N 66°-40'-15" W N. 67°15' W
50

148.43

(6) 11+06 $\frac{05}{\Delta}$ R 4°-05'-30" N 63°-46'-45" W N. 64°-30' W.
5

65.60

(5) 10+40 $\frac{45}{\Delta}$ R. 84°-30' N 67°-52'-15" W N. 68°-30' W.
N. 68°-32'-15" W.

129.55

Slope Vert. A.
163.30 -37°-30'

(4) 9+10 $\frac{9}{\Delta}$ R. 94°-42' S 27°-27'-45" W S 27-15 W

1/5/13

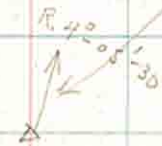
Sherman
Blaher
Keener

22
22

R. 62°-38
123-16
62-38

L. 2°-53'-30"
2 | 5°-47'
2 | 53-30

R. 4°-05'
2 | 8°-11
4-05-30



R. 84-31
2 | 168
84-30

R. 94-42
2 | 189-24
94-42
18-48
360
4 | 378-48
94-42

Cos. 37°-30' .79335
163.3
238005
238005
476010
79335
129.554055

Cos 37°-30' 9.899467
Log 163.3 - 2.212986
2.112453 - 129.55
27
183

F³ Line

Location Big Slide

(12)

20+73 $\overset{0}{\triangle}$ L. 46°-11'-30" S. 1°-36'-45" W. S. 1°-30' W.

46-11
92-25
46-11-30

209.16

232.4 Slope -26°-04'

(11)

18+63 $\overset{84}{\odot}$

56.54

(10)

18+07 $\overset{30}{\triangle}$ L 108°-53'-30" S 47°-38'-15" W S 47°-30' W
48'

223.12

(9)

15+84 $\overset{18}{\triangle}$ L. 19°-06' N 23°-08'-15" W N. 23°-45' W
18

-187.64

1/6/13 :
snowing hard

Sherman
Bloher
Keener

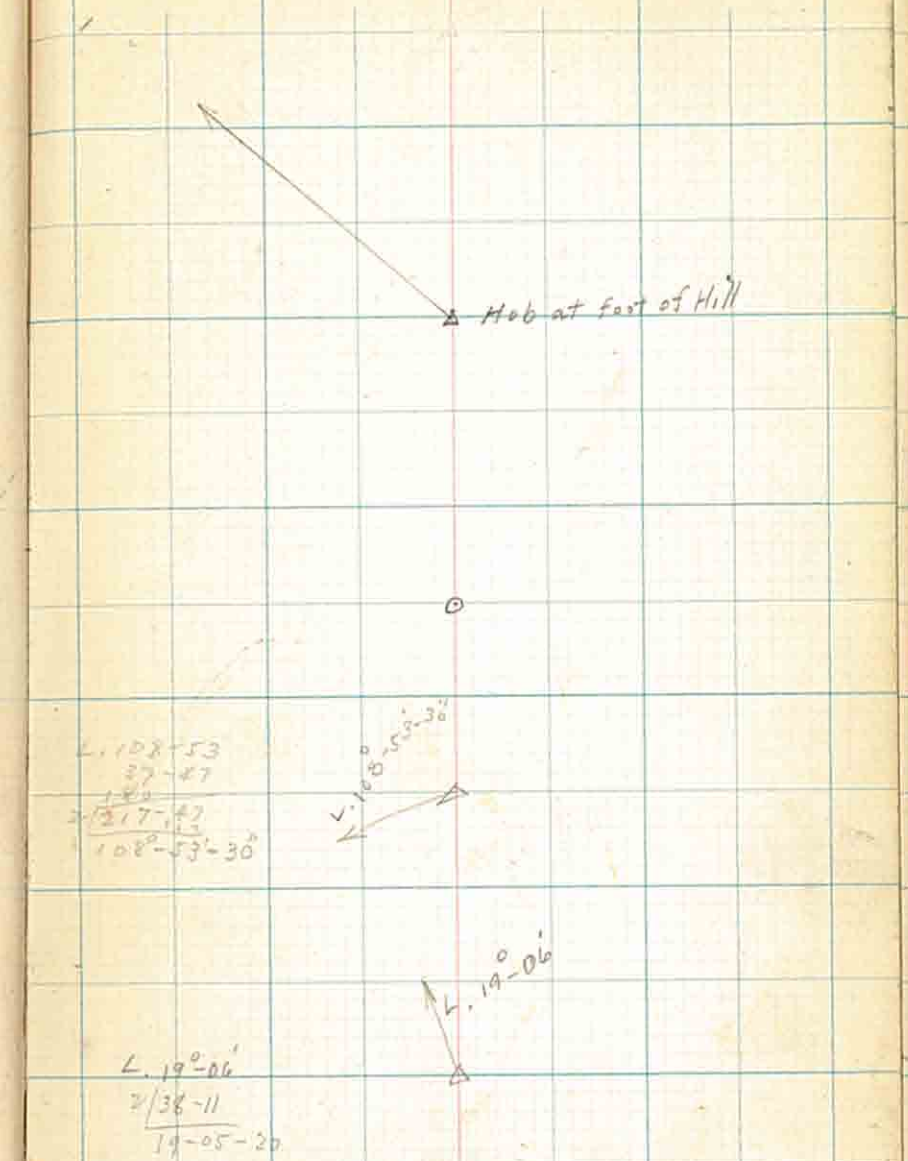
Hob at foot of Hill

L. 108-53
37-47
180
2)217-47
108°-53'-30"

L. 108°-53'-30"

L. 19°-06'

L. 19°-06'
2)38-11
19-05-20



F³ Line

Transit

(13) 27 + 92 6/Δ end

719.6

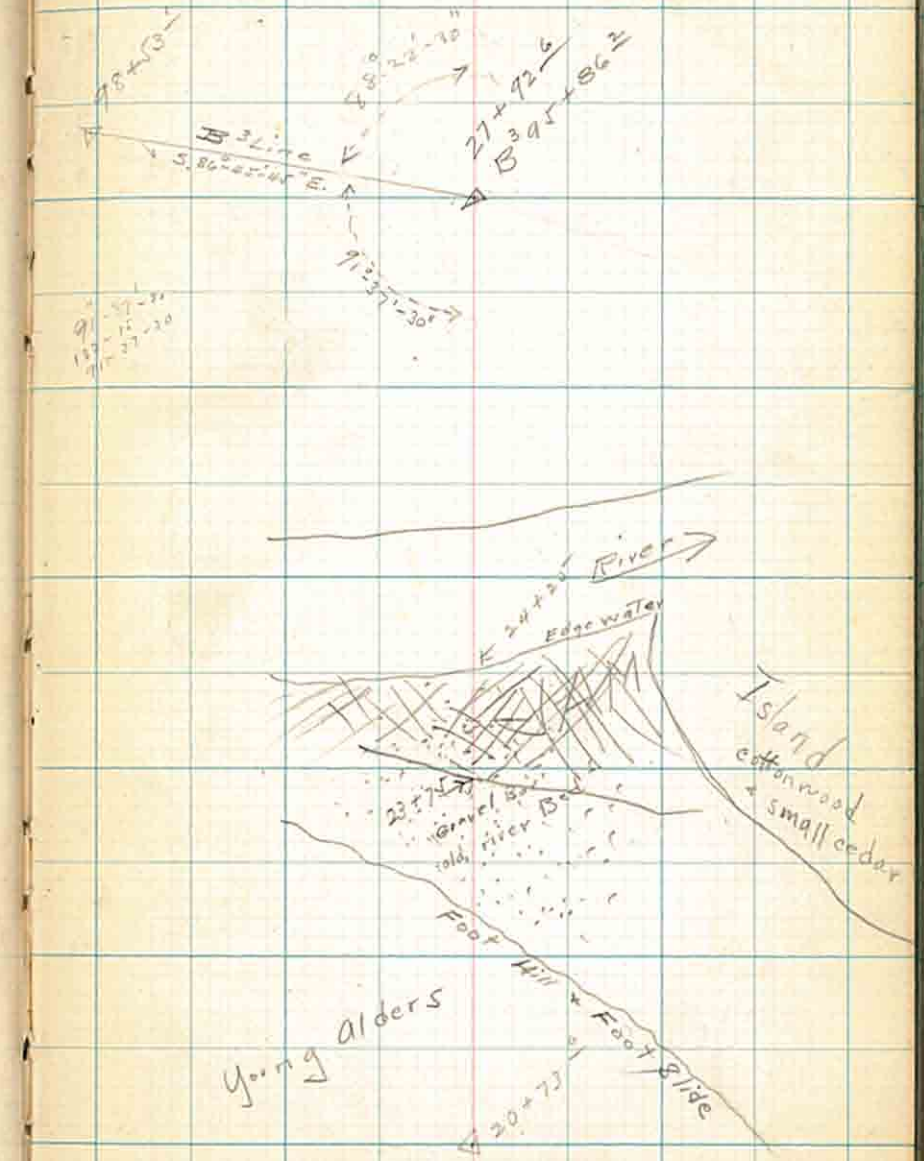
(14) 20 + 73 0/Δ

31°-36'-45" W. S. 1°-30' W.

2/13/13
Clear

Sherman
Bluher
Hart
Keener

24

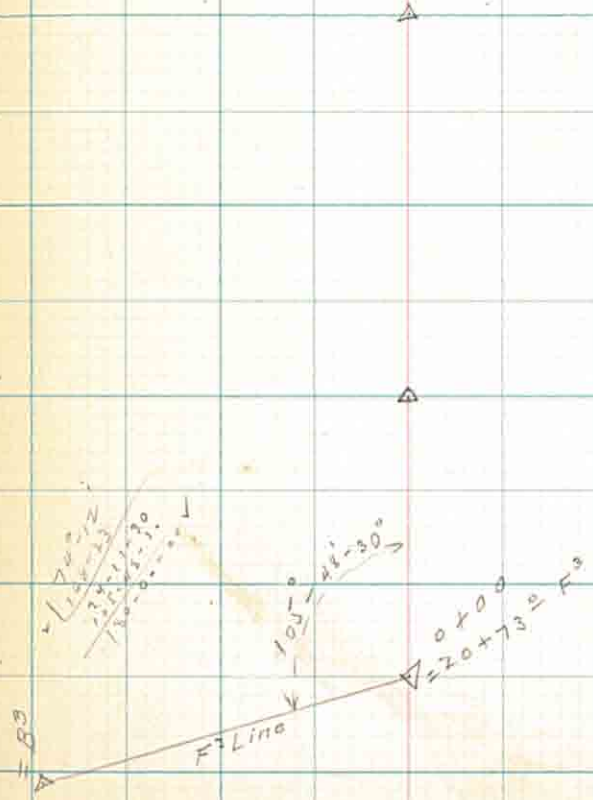


K³ Line | Transit | 2/13/13 | Sherman Bluher Hart Keener | 235

12+32 $\frac{V}{\Delta}$ end

4+26 $\frac{3}{\Delta}$ R 0°-07'

0+00 Δ N. 73° W.



K³ Line

Levels

		H.I.		
		164.97		
0+35	9.8	5.1	155.2	
TP	-12.82		152.15	
	+ 0.04	152.19		
		.2		
0+50	3.5		148.7	
1+00	11.6		140.6	
2	8.4		143.8	
3	10.7		141.5	
TP Rock	-10.60		141.59	Near Sta. 3
	+ 6.0	147.59		
		.6		
4	4.9		142.7	
+26 3/△	6.10		141.49	
5	7.6		140.0	
6	12.4		135.2	
TP Peg	-9.35		138.24	
	+ 2.50	140.74		
7	4.8		135.9	
8	7.6		133.1	
9	4.6		136.1	
+50	3.5		137.2	Top bank branch White R.
+65	10.2		130.5	edge water
10+00	10.6		130.1	
+50	6.4		134.3	Top bank
11+00	4.4		136.3	
12	5.6		135.1	
TP +32 5/△	-5.98		134.76	on hub

2/10/13

Sherman Hart

A^3 Line Levels on A^3 Line

Sta.	Rod	H.I.	Elev.	B.S.	F.S.
B.M.	+3.40	103.40	100.00		
Bl36 +00	5.0		98.4		
Bl37 +00	7.5		95.9		
TP Rock	-11.03		92.37		
	+8.12	100.49			
A^3 2+00	2.8		97.7		
3+00	6.5		94.0		
+80	3.5		97.0		
TP3+90 $\frac{40}{\Delta}$ ⊙	-3.97		96.52		
	+4.96	101.48			
4+00	11.6	.5	89.9		
5+43	11.5		90.0		
6+00	7.4		94.1		
+09 $\frac{0}{\Delta}$			94.86 — on hub		
7	7.6		93.9		
8	7.0		94.5		
+90	4.3		97.2		
TP Pig.	-1.80		99.68		
	+7.03	106.71			
9+00	2.7		104.0		
+30 $\frac{20}{\Delta}$	2.47		104.24		
10	7.0		99.7		
+50	7.1		99.6		
+75	10.6		96.1		
11	10.4		96.2	B.S.	F.S.
12	10.4		96.2	3.40	11.03
TP Rock	-10.34		96.37	8.12	3.97
	+11.12	107.49		4.96	1.80
13	13.5	.5	~~100~~ 94.0	7.03	10.34
14	9.5		98.0	11.12	27.14
15	11.3		96.2	34.63	
16	10.3		97.2	27.14 F.S.	
17	4.2		103.3	7.49 Diff. B.M.	✓
18	6.3		101.2	100.00	
				107.49 H.I.	

1/10/13 A^3 Line Sherman Hart 277

Cottonwood tree

Auburn Pk Blvd.

Rock near Rd.

Top of Bulkhead Brush - concrete ⊙ 3+90 $\frac{40}{\Delta}$

Top of water at edge of Bulkhead 1/10/13

Edge water top 1/10/13

River

Foot of Bank

Top bank on Hub

Top Bank Foot "

A3 Line — Levels for Topog. — 4/9/13

		H. I.				
		107.49				
P19+00 49 Δ	-5.52		101.97			on Hub
	+10.81	112.78				
20	10.3	.9	102.5			
21	12.5		100.4			
22	15.5		97.4			
+56	15.0		97.9			Foot Bank
+65	11.7		101.2			
+73	5.2		107.6			Top bank
23	3.5		109.4			
24+00 00 Δ	-4.27		108.51			
	+6.40	114.91				
25	5.7		109.2			
26	4.0		110.9			
26+67 35 Δ	3.50		111.40			on Hub
27	4.4		110.5			
+49	4.8		110.1			
28	8.0		106.9			
+62	3.2		111.7			
29	7.4		107.5			
30	2.5		112.4			
TP Pg	-2.16		112.75			
	+4.53	P17.28				
30+46 03 Δ	4.82		112.46			on Hub
31	10.9		106.4			
32	4.9		112.4			
33	5.3		112.0	4.27		
34	5.3		112.0	2.16		
35	4.0		113.3	5.44		
36	5.6		111.7	11.87		
37	5.3		112.0			
TP Pg	-5.44		111.84			
	+7.33	119.17				

B.S.
10.81
6.40
4.53
7.33
29.07
11.87
diff 17.20
B.M. 101.97
119.17

A³ Line — Levels on A³ Line

		119.17			
38 + 0.0	4.9		114.3		
38 + 60 $\frac{0}{0}$	4.33		114.84		on Hub
38 + 85	6.4		112.8		Top of Bank
39 + 00	13.6		105.6		Foot of Bank creek 2½' deep
+ 33	13.5		105.7		Foot of Bank
+ 40	6.6		112.6		Top bank
40	7.0		112.2		
41	3.9		115.3		
42	5.1		114.1		
TP + 77 $\frac{45}{\Delta}$	-3.50		115.67		
	+5.31	120.98			
43	5.7		115.3		
44	5.8		115.2		
45	4.8		116.2		
+ 73	4.2		116.8		Top bank
46	8.7		112.3		in Riverbed
47	4.6		116.4		
TP + 33 $\frac{80}{\Delta}$	-4.84		116.14		on hub
	+5.84	121.98			
B.M.	0.47		121.51		across River on Joe Bobs Place
48	7.1		114.9		
+ 50	4.4		117.6		Top Bank
49	4.2		117.8		
50	4.9		117.1		
51	3.0		119.0		
TP	-2.90		119.08		
	+6.66	125.74			
52	5.9		119.8		
53	5.4		120.3		
B.M. + 76 $\frac{88}{\Delta}$	4.61		121.13		
54	4.7		121.0		
54 + 30	6.		119.7		Top Bank slough running Water

F.S. 4.84 2.90 / 7.74

B.S. 5.31 5.84 6.66 / 17.81 7.74 / 10.07 / 115.67 / 125.74

A³ Line

Levels

		125.74	
55 + 10	7.5		118.2
56	4.2		121.5
57	5.0		120.7
TP peg	− 4.94		120.80
	+ 8.07	128.87	
58	7.7		121.2
59	6.1		122.8
+ 16 25/△	4.95		123.92
60	4.8		124.1
61	6.4		122.5
62	5.1		123.8
62 +			
63	2.5		126.4
64	2.8		126.1
TP	− 2.40		126.47
	+ 7.64	134.11	
65	7.3		126.8
66	6.6		127.5
67	5.6		128.5
68	4.7		129.4
69	5.5		128.6
70	3.6		130.5
71	2.3		131.8
TP peg	− 1.77		132.34
Near 71+74 60/△	+ 5.16	137.50	
72	6.1		131.4
7 35	5.2		132.3
73 + 35	12.6		124.9
74	10.0		127.5
75	10.2		127.3
+ 32	12.5		125.0
76	4.5		133.0
77	4.1		133.4

B.S. 8.07 7.64 5.16 20.87 4.17 16.70 120.80 137.50

F.S. 2.40 1.77 4.17

1/21/13

Top bank

Top bank

near Hub

Top Water + edg of water in River

Top Bank

A³ Line

Levels

		H. I.		
		137.50		
TP 77+94 70/Δ	-3.59		133.91	on hub
	+7.78	141.69		
78	8.1		133.6	
+95	15.0		126.7	
80	7.7		134.0	Top Bank River
81	6.5		135.2	
+11+45	4.82		136.87	on Hub
82	3.5		138.2	
83	5.2		136.5	
84	6.0		135.7	
TP 85 peg	2.5 / -2.35		139.2 / 139.34	
	+5.33	144.67		
86	5.6		139.1	
+76	6.3		138.4	Top of bank
87				
88				
89				
90	3.7		141.0	
91	3.7		141.0	
TP alder Sp	-1.21		143.46	
	+3.66	147.12		
92	5.5		141.6	
93+00 0/Δ	4.50		142.62	on hub
94	4.4		142.7	
95	4.5		142.6	
TP top stake	-3.45		143.67	Sta. 95+00
	+6.57	150.34		
96	7.8		142.5	
+55	15.7		134.6	
97			137.1	
98			138.2	
99			139.7	
100			139.7	
101	4.2		146.1	
101+65 92/Δ	0.34		150.00	
B.M.	0.93		149.41	on Fir 40' R 101+25 B.M.

B.S. 7.78 5.33 3.66 6.57 23.44 7.01

F.S. 2.35 1.21 3.45 7.01

Diff. 16.43 B.M. 133.91 150.34

210.33 149.41 60.92

on Right Bank of
Put B.M. across River near W. end high bank at foot of Big Slide 1 H.I. 150.34 Rod reading 2.54
Elev B.M. on small stump 147.80

1/21/13

Sherman Hart

A³ Line — Levels for Topog

	Rod	H.I.	Elev.	
0+00 B.M. Hub	+3.80	112.31	108.51	
1	7.7		104.6	
2	8.7		103.6	
3	8.7		103.6	
4	6.2		106.1	
4+13 $\frac{80}{\odot}$	5.50		106.8	
5	2.4		109.9	
6	2.6		109.7	
TP peg	-3.92		108.39	
	+7.20	115.59		
6+71 $\frac{70}{\triangle}$	3.42		112.17	
7	4.8		110.8	
8	5.3		110.3	
9	2.3		113.3	
TP9+83 $\frac{80}{\triangle}$	-2.90		112.69	
	+2.76	115.45		
10+00	5.2		110.2	
11	3.1		112.3	
12	9.4		106.0	
13	6.0		109.4	
TP13+29 $\frac{90}{\odot}$	-4.58		110.87	
14	+4.76	115.63		
15	5.5		110.1	
	8.0		107.6	
16+55 $\frac{2}{\triangle}$	7.7		107.9	
17	11.2		104.4	
18	19.0 Mort the ground		96.6	
19	13.0		102.6	
20	10.8		104.8	
21	10.8		104.8	
+74 $\frac{2}{\text{Stake}}$	11.1		104.5	end

1/9/13 — Sherman Hart — 32

= Hub 24+00 A³ Line

B.M. on Hub

on Hub

on Hub

on Hub

B^3 Line B^3 Line Levels

B.M.			99.68
	+ 0.91	100.59	
6+00	8.2	.6	92.4
7+00	8.1		92.5
8	7.5		93.1
9	9.5		91.1
TP peg	- 1.79		98.80
	+ 6.13	104.93	
9+50	7.4		97.5
10	7.6		97.3
+58 45 △	1.58		103.35
10+65	1.9		103.0
+80	8.0		94.9
11	11.3		93.6
12	12.4		91.5
13	10.5		93.8
14	9.0		95.9
15	8.8		96.1
16	6.4		98.5
17	5.9		99.0
TP +77 △	-6.85		98.06
	+9.78	107.86	
18	9.6	.9	98.3
19	8.4		99.5 x
20	8.6		99.3
21	8.2		99.7
22	7.9		100.0
23	7.9		100.0
24 +00 0 △	-4.42		103.44
25			
26	5.0		102.9
26+85	5.9		102.0
28	1.8		106.1

1/28/13
cold Foggy

Sherman
Hart

Peg foot of bank near 8+90 A^3 Line Page 27

Foot bank

B³ Line

Levels

		107.86	
TP 29+00 0/△	−1.68	.0	106.18
	+5.22	111.40	
30	5.6		105.8
31			
32	4.4		107.0
33	-		
34	2.7		108.7
TP	−0.68		110.72
	+10.07	120.79	
35	8.1	.8	112.7
36	11.7		109.1
37	9.4		111.4
38	10.0		110.8
BM, +46 8/△	5.05		115.64
38+85	8.8		112.0
40	8.9		111.9
TP	−1.08		119.71
	+4.43	124.14	
41	9.9		114.2
+36 0/△			
42	10.4		113.7
43+40	13.8		110.3
44	11.8		112.3
TP +52 1/△	−3.54		120.60
	+5.84	126.44	
45	6.0		120.4
46	5.0		121.0
47	5.5		120.9
48	5.0		121.4
+35	6.0		120.4
+55	11.0		115.4
+65	12.2		114.2

+ 5.22
10.07
4.43
5.84
25.56
5.30
20.26
106.18
126.44 ✓

− 0.68
1.08
3.54
5.30

1/28/13

Sherman Hart

Tack in Big Fir Log

on big Fir Log.

edge creek

Top bank

Edge and top of water of creek 1' deep x 30' wide

mud on bottom

1/29/13 Sherman Hart

Foggy mist Tem. 40° F.

B³ Line		Levels		
		4.1		
		126.44		
49	9.4		117.0	
50	6.1		120.3	
51	4.2		122.2	
52	2.1		124.3	
TP peg	-1.68		124.76	
	+4.05	128.81		
52 +91 5/Δ	4.55		124.26	
53	8.1		120.7	
54	6.1		122.7	
55	6.0		122.8	
56	6.5		122.3	
TP +54 4/Δ	- 4.52		124.29	
	+9.42	133.71		
57	9.7		124.0	
58	8.7		125.0	
59	4.7		129.0	
+ 40	10.9		122.8	
60	8.7		125.0	
TP + 94 8/Δ	-3.59		130.12	
	+6.69	136.81		
61	6.8		130.0	
62	12.6		124.2	
63	7.5		129.3	1
64	4.7		132.1	4.03
65	4.0		132.8	4.47
66	5.1		131.7	6.69
+ 27 5/Δ	- 5.20		131.61	
	+4.20	135.61		
67	3.9		131.7	
68	4.6		131.0	
69	5.7		129.9	
70	6.5		129.1	
71 + 70	7.0		128.6	
	5.9		129.7	
+ 35 7/Δ	4.90		130.71	

top bank

near 52+00

on hub

edge of top water creek 1.2' deep × 35' wide

on hub

on hub

top water in coal creek.

B^3 Line — Levels

	Rod +	Rod −	H.I.	Elev.
7			125.61	
72	5.4			130.2
73	5.8			129.8
74	4.7			130.9
75	4.1			131.5
TP +60 $\frac{2}{\Delta}$		− 0.81		130.80
	+10.18		140.95	
76	9.5		141.0	131.5
77	8.6			132.4
78	7.8			133.2
79	7.3			133.7
80	8.7			132.3
81 +	10.4 9.1			131.9
82	4.9			136.1
+ 07 $\frac{4}{\odot}$				
83	4.0			137.0
84	3.4			137.6
85	4.0			137.0
86	3.2			137.8
87	3.8			137.2
TP +35 $\frac{6}{\Delta}$		− 3.66		137.32
	+ 7.54		144.86	
88	8.2		.9	136.7
+ 50	10.6			134.3
89	5.1			139.8
90	4.4			140.5
+ 94 $\frac{3}{\Delta}$	4.8			140.1
91	4.8			140.1
92	5.2			139.7
93	3.6			141.3
94	3.6			141.3
95	2.5			142.4
TP. +86 $\frac{2}{\Delta}$		− 1.45		143.41
	+8.62		152.03	
B.M.	2.60			149.43

1/30/13

Sherman Hart

Top water in creek

Top water in creek

Fir tree 1' dia. 40' R 50.101+25 A^3 Line

J³ Line

Levels

Transit on page 8

		H. I.		
B. M.	+4.65	99.51	94.86	hub 6+09 A³ Line P7
1	5.2		94.3	
2	6.3		93.2	
3	6.7		92.8	
4	7.5		92.0	
5	7.7		91.8	
TP	-7.48		92.03	
	+9.23	101.28		
6	8.9		92.4	
+80	10.2		91.1	edge coal creek and top. bank
7+90	12.65		88.7	edge " " and top of water
8	10.9		90.4	
+20	3.6		97.7	Top Bank
9	4.9		96.4	
9+38 2/Δ	4.70		96.58	on hub
10	3.1		98.2	
11	3.5		97.8	
TP	-4.25		97.03	
	+4.56	101.59		
12.	5.0		96.6	
13	3.8		97.8	
14	4.6		97.0	
+16 0/0	4.59		97.00	
15	8.3		93.3	
TP +	-12.10		89.49	
15+50.	+3.41	92.90		Foot bank
→	4.30		88.6	
16+00	5.2		87.7	
+93 6/Δ	4.54		88.36	on hub
17	4.6		88.3	
18	5.2		87.7	
19	9.6		83.3	edge water in branch R.
+05	10.0		82.9	

2/4/13

Sherman Hart

J 3 Line 1

Levels

H. I.
92.90

20	10.6	82.3
21	10.2	82.7
22	10.7	82.2
23	11.4	81.5
24	12.3	80.6
25	13.3	79.6
+83 $\frac{1}{\Delta}$	-9.73	83.17

2/4/13

Sherman Hart

δ^3 Line

Levels

Transit on Page 9

B. M.	+ 6.86	109.71	103.85
0 + 00	15.90		93.8
1 + 00	14.4		95.3
+ 10	6.2		103.5
+ 33 3/10	4.56		105.15
2 + 00	5.0		104.7
3	9.4		100.3
4	5.4		104.3
5	5.3		104.4
6	3.5		106.2
7	4.4		105.3

2/4/13

Sherman Hart

hub B^3 Line 10+58 45

on sidehills

Top Bank

on hub

e^3 Line — Levels

Transit on page 10

B. M.	+6.27	104.35	98.08
0 + 00	4.55		99.80
1 + 00	7.1		97.2
2	7.7		96.6
TP	-2.63		101.72
	+10.20	111.92	
2+65	8.2		103.7
3 + 00	4.7		107.2
3 + 10	4.32		107.60
4 + 00	4.1		107.8
5 + 00	4.6		107.3
+ 47	-3.64		108.28
	+5.55	113.83	
6	6.0		107.8
7	5.0		108.8
+80	10.1		103.7
+99 ±Δ	4.59		109.24
8	4.6		109.2
9	6.6		107.2
10	7.2		106.6
11	8.1		105.7
T. P.	-8.19		105.64
	+7.53	113.17	
12	8.2		105.0
+75	4.6		108.6
13	9.4		103.8
14	9.3		103.9
+20	7.3		105.9
+50	13.5		99.7
15	10.0		103.2

h.b 17+66 A^3 Line P. 33

Peg at stat 11+00

Edge of Riverbank

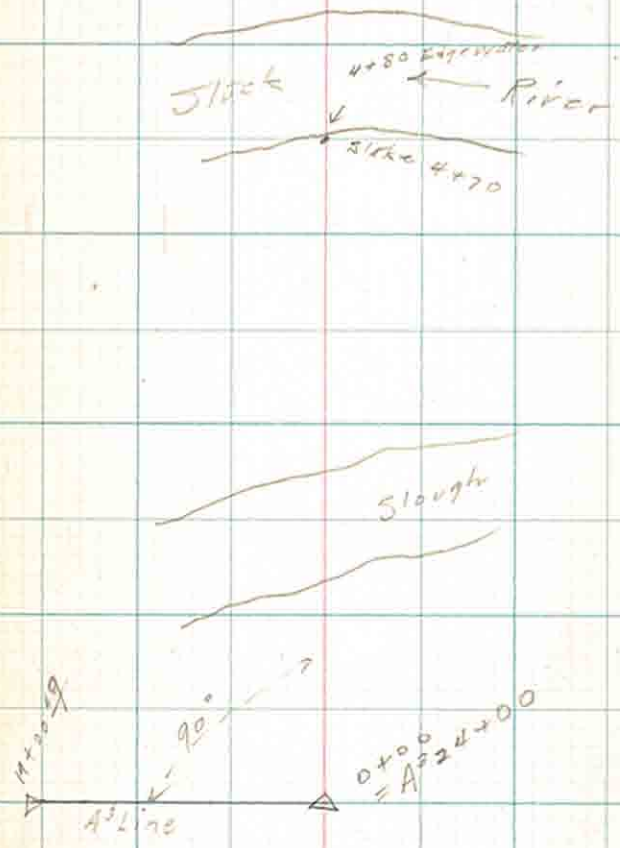
J³ Line

4+70 stake

0+00 △

7/8/13

Sherman
Hart
Bluher
Keener



f³ Line Transit

19+31.³ Stake end

15+88 2/⊙

10+76 8/⊙

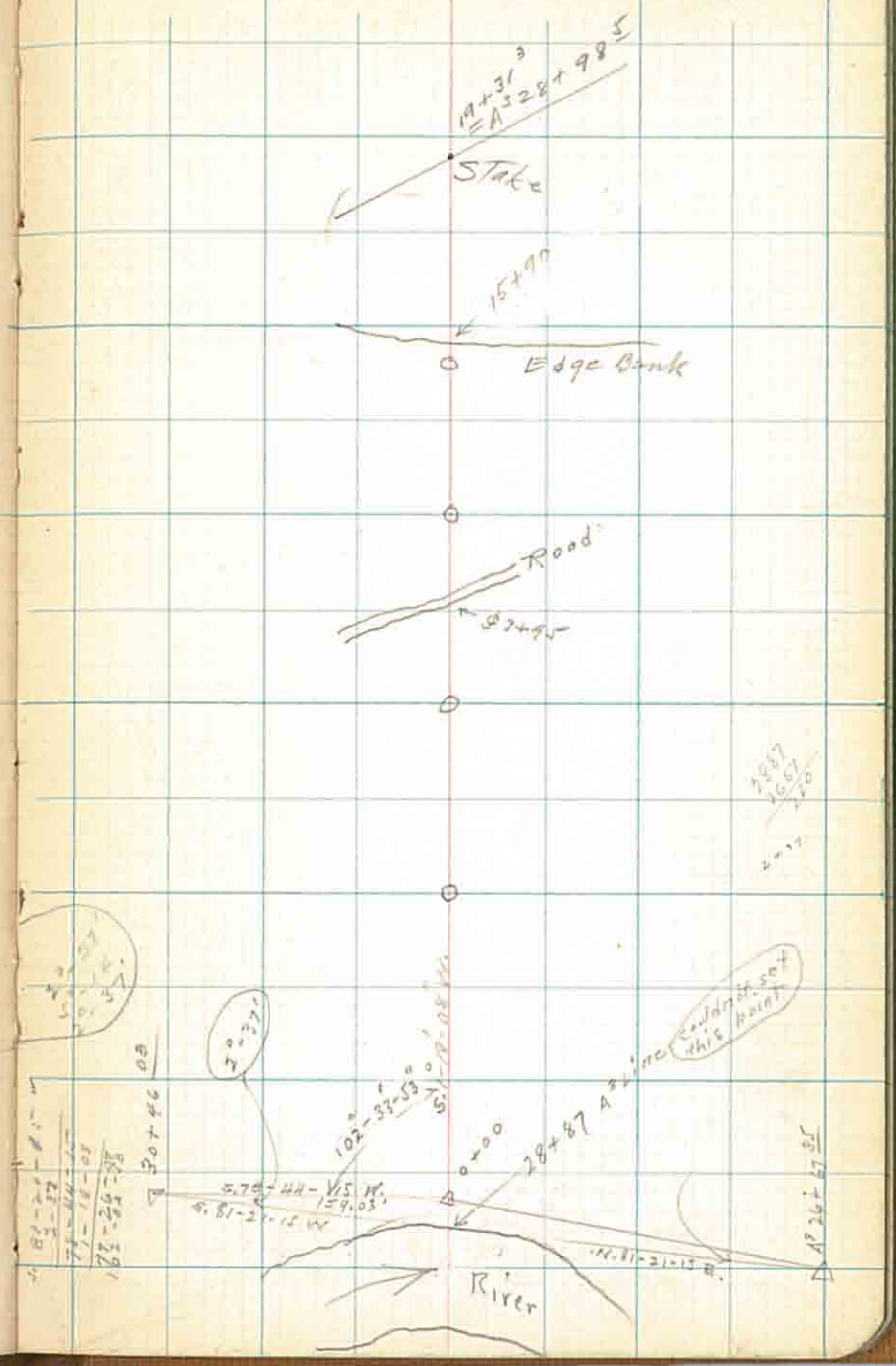
4+91 2/⊙

1+23 0/⊙

0+00 △ S.1° W

2/8/13

Sherman
Bluher
Hart
Keener



g³ Line

Transit

20 + 38 end

15 + 04 8/△ L. 0°-44'

13 + 07 1/⊙

9 + 60 1/△ R. 1°-34' North

8 + 60 1/△ L. 3°-08' 100'

7 + 60 1/△ R. 1°-34' 100'

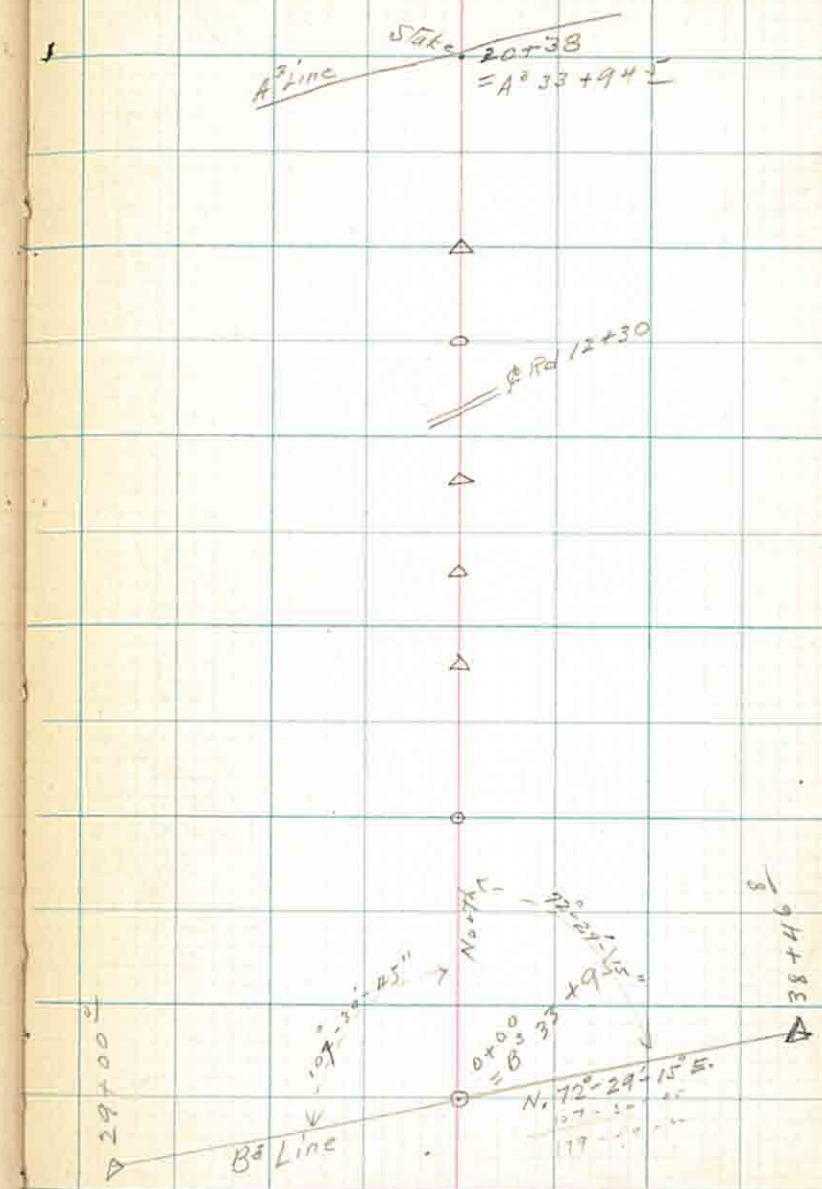
1°-34'
3°-08'
1°-34'

4 + 43 5/⊙

0 + 00 ⊙ North

2/8/13
Clear Sunshine
Cold

Sherman
Bluher
Hart
Keener



h^3 Line — Transit

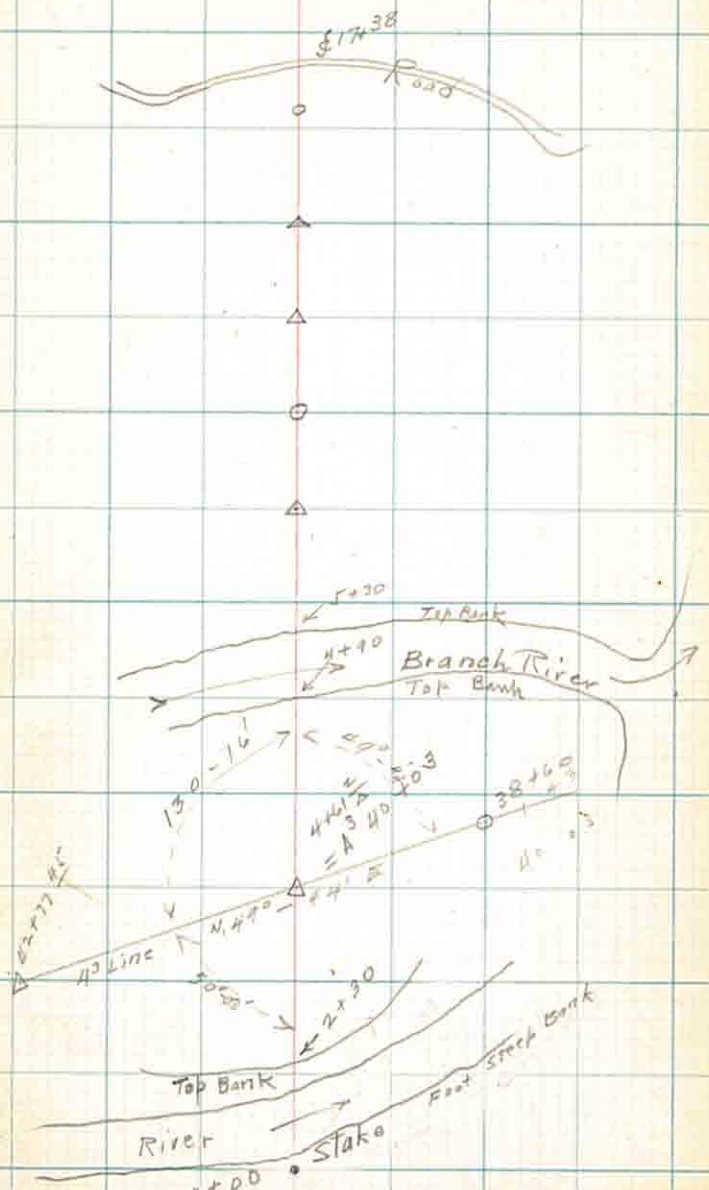
19+14 $\frac{4}{\odot}$		
17+00 $\frac{0}{\odot}$		
14+37 $\frac{7}{\triangle}$	R. 2°-32'	South
11+37 $\frac{7}{\triangle}$	L. 5°-04'	S. 2°-30' E
10+37 $\frac{7}{\odot}$		
8+37 $\frac{7}{\triangle}$	R. 2°32'	S. 2°30' W
4+61 $\frac{2}{\triangle}$	R. 0°-19'	South
0+00 •	Stake edge Rt Bank River	

2°-32'
5-04
2-32

2/10/13

Sherman
Bluher
Hart
Keener

44



h^3 Line

Transit

27 + 37 $\frac{3}{}$ stake end

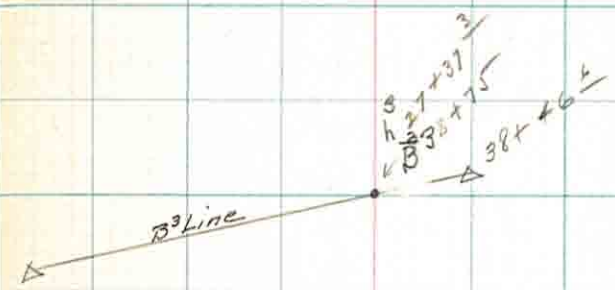
23 + 79 $\frac{3}{\odot}$ South

22 + 64 $\frac{5}{\odot}$ on line South

2/10/13

Cold A.M. Clear Sunshine

Sherman
Bluher
Hart
Keener



i^3 Line

Transit

18+10 $\frac{3}{\odot}$

14+15 $\frac{2}{\odot}$

9+68 $\frac{6}{\odot}$

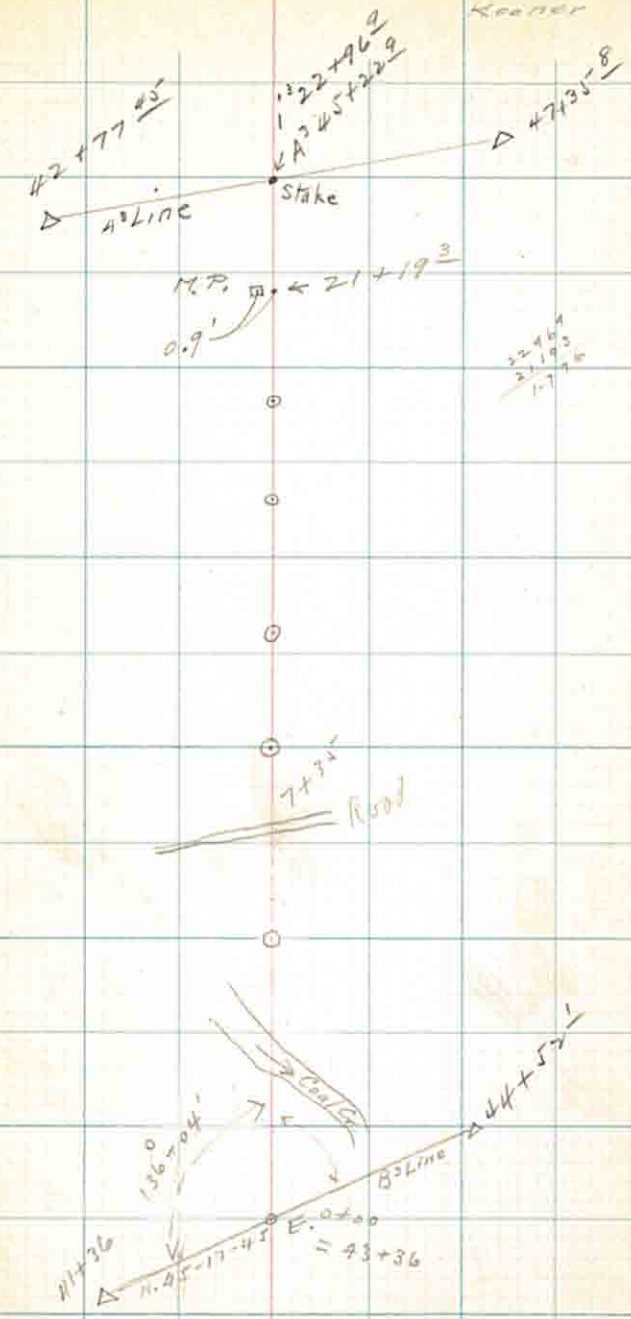
8+49 $\frac{8}{\odot}$

4+65 $\frac{8}{\odot}$

0+00 $\odot$ N.1-21-A5E

4/11/18

Sherman
Bluker
Hart
Keener



K 3 Line

15+75 4 end

13+07 7/0

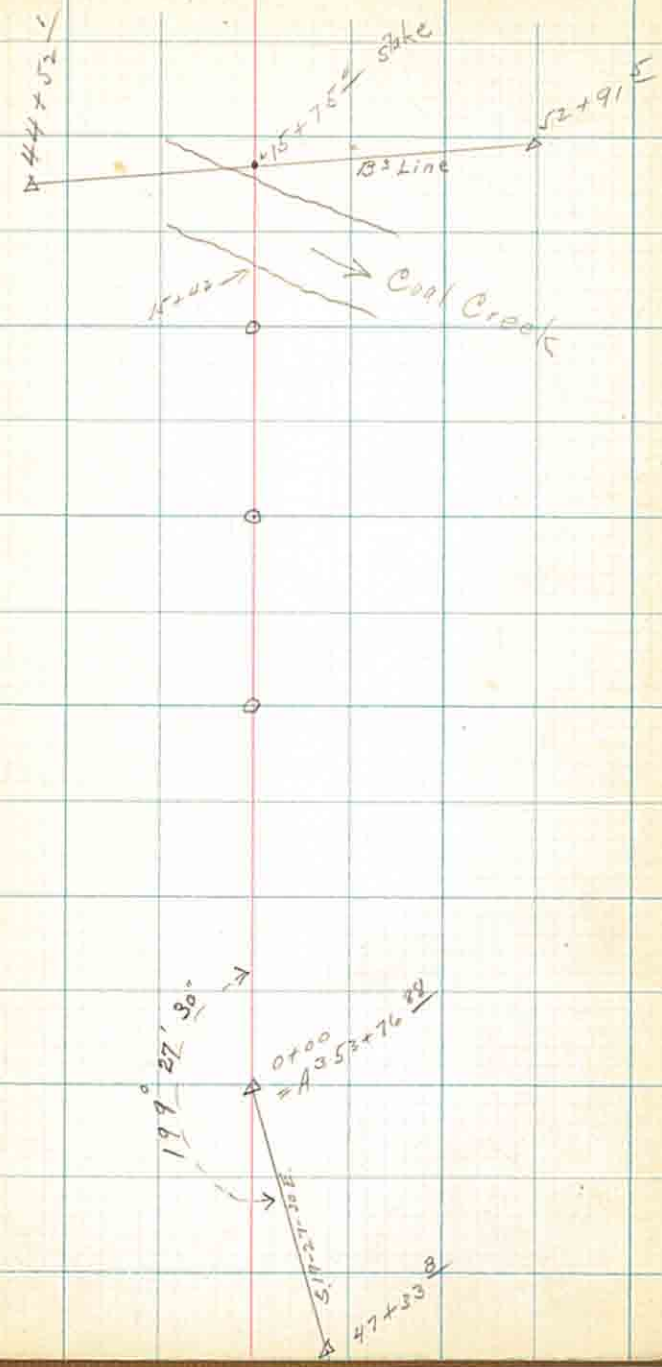
10+09 0/0

4+59 5/0

0+00 0/A

2/11/13
clear Sun.

Sherman
Bluher
Hart
Keener



S^3 Line

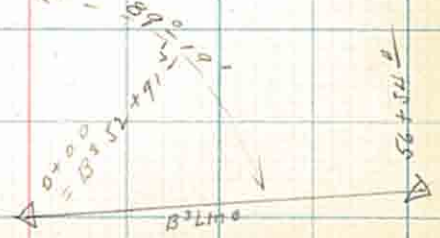
12+01 stake End

3+74 $\frac{0}{0}$

0+00 △ S. 0°-15' E.

2/12/13

Sherman
Bluber
Hart
Keener



M^3 Line.

11+39.5 end stake

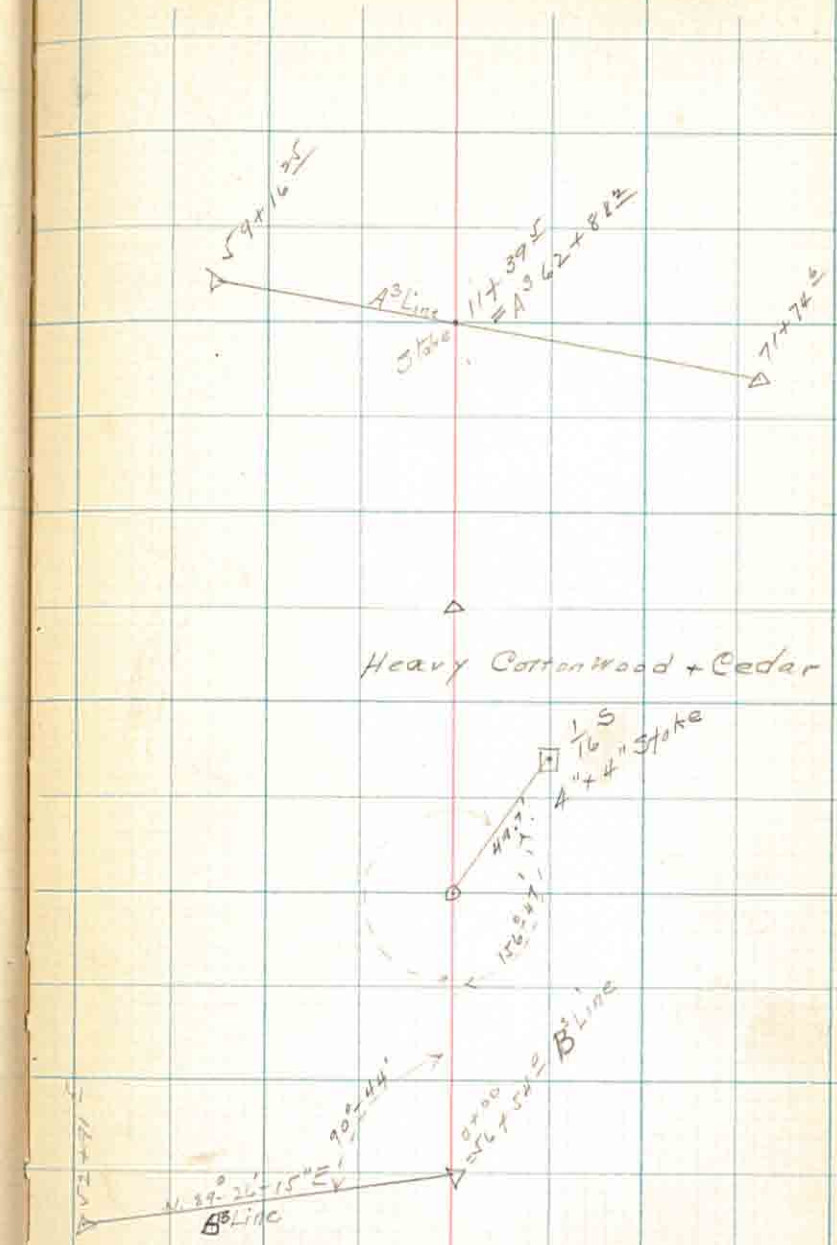
8+32 $\frac{2}{\triangle}$ L. 0°-23'

2+52 $\frac{0}{\odot}$

0+00 $\frac{0}{\odot}$

2/12/13

Sherman
Bluher
Hart
Keener



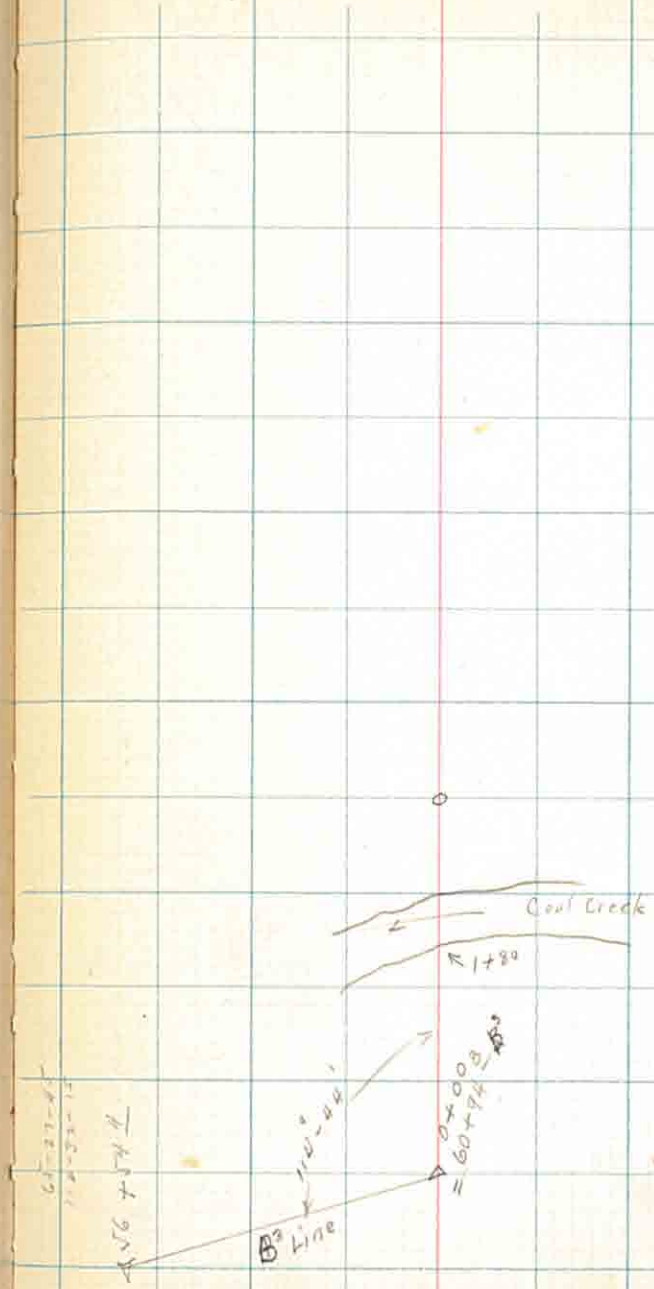
n³ Line

4+04 1/0

0+

2/12/13

Sherman
Bluher
Hart
Koerner



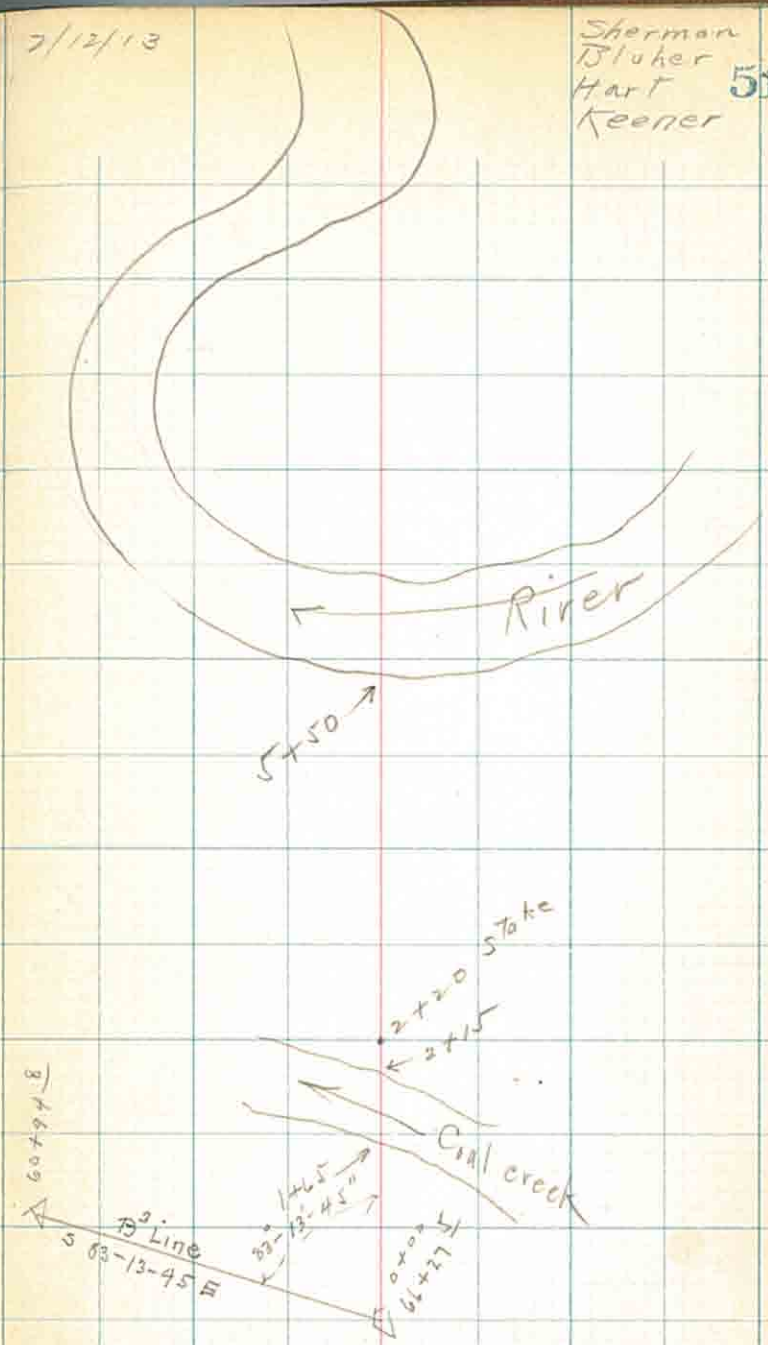
O^3 Line

5+50 end

0+00 $\frac{0}{0}$

7/12/13

Sherman
Bluher
Hart
Keener

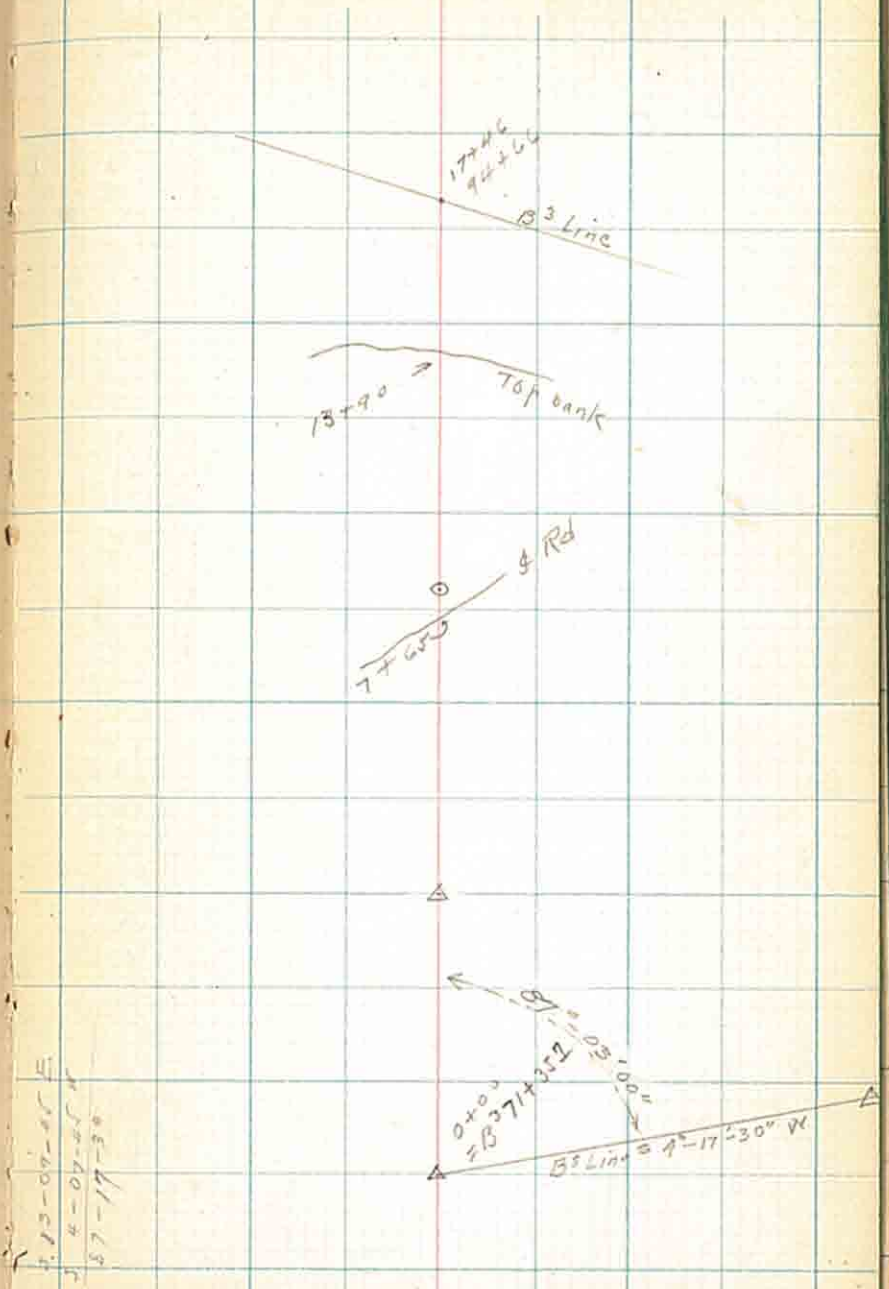


p³ Line

17+46	end		
7+75 6/⊙			
3+24 6/△	L, 0°-13'		S, 83°30'E
0+00			S. 83° E

2/12/13

Sherman
Bluher
Hart
Keener



F Line Levels

	Rod	U.I.	Elev.
B.M.	+6.00	153.80	147.80
24+25	16.1		137.7
24+00	11.5		142.3
23	10.6		143.2
22	9.4		144.4
21+60	4.0		149.80
TP	-1.63		152.17
	+12.80	164.97	
21+00	7.0		158.0
20+73 ○/△	-3.15		161.82
	+12.52	174.34	
20+55	7.4		166.9
TP peg	-0.06		174.28
	+12.84	187.12	
20+35	12.7		174.4
20+15	4.5		182.6
TP Rock	-0.04		187.08
	+12.95	200.03	
20+00	10.7		189.3
19+85	3.0		197.0
TP Rock	-0.21		199.82
	+13.06	212.88	
19+60	6.9		206.0
TP	-0.25		212.63
	+12.80	225.43	
19+45	11.8		213.6
+25	2.9		222.5
TP	-0.30		225.13
	+12.46	237.59	
19+10	5.6		232.0
TP	-0.25		237.34
19+00	+12.96	250.30	
	11.1		239.2

7/13/15

Sherman
Hart
Keener

Top & edge of water in River

on hub

F³ Line — Levels — 2/19/13 — Sherman Keener

		250.30		
18+85	2.5		247.8	
TP	−0.20		250.10	
	+12.70	262.80		
18+75	4.5		258.3	
TP	−0.06		262.74	
	+13.13	275.87		
18+63 84/⊙	7.59		268.28	on hub
18+50	2.4		273.5	
TP	−0.42		275.45	
	+5.10	280.55		
18+07 30/△	0.73		279.82	on hub
17+30	7.0		273.5	
17+00	9.9		270.6	
16+40	10.4		270.1	
16+00	12.5		268.0	
TP	−13.18		267.37	
	+0.73	268.10		
15+84 18/△	3.56		264.54	on hub
15+50	9.5		258.6	
TP	−12.26		255.84	
	+0.0	255.84		
15+00	4.3		251.5	
14+00	13.8		242.0	
13+96 54/△	13.90		241.94	on hub
TP	−13.00		242.84	stake near hub
	+12.30	255.14		
13+50	10.1		245.0	
13+35	5.1		250.0	
13+25	0.1		255.0	
TP	−0.06		255.08	
	+13.00	268.08		
13+10	6.9		261.2	
13+00	3.2		264.9	

F³ Line

Levels

		268.08		
12+85	0.8		267.3	
TP	-0.12		267.96	
	+12.92	280.88 .9		
12+70	7.9		273.0	
12+54 48 △	3.38		277.50	on hub
12+34	7.6		273.3	
12+25	13.7		267.2	
12+00				in bottom Gulch
11+25	5.1		275.8	
TP	-0.12		280.76	
	+13.01	293.77 .8		
11+20	13.2		280.6	
+06 05 △	3.89		289.88	on hub
11+00	3.9		289.9	
TP 10+40 45 △	-7.25		286.52	hub begin steep slope up hill
	+12.83	299.35		
TP	-0.09		279.26	
	+13.20	312.46		
10+00	0.1		312.4	
TP	-0.25		312.21	
	+12.91	325.12		
TP	-0.08		325.04	
	+12.72	337.76		
TP	-0.15		337.61	
	+13.25	350.86		
TP	-0.12		350.74	
	+13.02	363.76		
TP 9+35	-0.07		363.69	Rock on ground begin steep slope up hill
	+13.00	376.69		
TP	-0.60		376.09	
	+12.67	388.76		
9+10 9 △	3.73		372.36	hub

2/17/13

Sherman Keener

F^3 Line		Levels		
		388.76		
TP8 + 22 $\frac{3}{\Delta}$	− 4.80		383.96	on hub
	+ 3.90	387.86		
8 + 00	4.7	.9	383.2	
7 + 00	4.4		383.5	
6 + 00	6.2		381.7	
TP5 + 61 $\frac{1}{\Delta}$	− 6.45		381.41	on hub
	+ 2.83	384.24		
5 + 00	9.2		375.0	
4 + 31 $\frac{9}{\Delta}$	4.65		379.59	on hub
4 + 00	7.1		377.1	
TP	− 12.16		372.08	
	+ 0.13	372.21		
3 + 00	3.5		368.7	
2 + 84 $\frac{4}{\Delta}$	4.50		367.71	
2 + 00	7.7		364.5	
TP	− 1.79		370.42	
	+ 12.75	383.17		
1 + 70	13.0		370.2	
1 + 00	11.2		372.0	
TP	− 2.05		381.12	
	+ 6.20	387.32		
0 + 00 $\frac{0}{\Delta}$	4.10		383.22	on hub top hill above slide

2/19/13

Sherman
Keener

D 3 Line Levels

Transit on Page 19

	Rod	H.I.	Elev.
B.M.	+8.94	130.45	121.51
0+00 $\frac{0}{\Delta}$	4.33		126.12
1	5.5		124.9
2	3.5		126.9
3	3.6		126.8
TP	-2.92		127.53
	+4.88	132.41	
4	5.6		126.9
5	5.9		126.5
+81 $\frac{8}{\Delta}$	4.74		127.67
+90	8.2		124.2
6	13.0		119.4
7	12.0		120.4
8	10.0		122.4
9	8.1		124.3
10	6.3		126.1
11	5.3		127.1
TP +28 $\frac{7}{\Delta}$	-5.20		127.21
	+6.80	134.01	
12	6.0		128.0
13	6.8		127.2
14	5.7		128.3
+91 $\frac{1}{\Delta}$	5.20		128.8
15	5.0		129.0
16	4.4		129.6
TP 17+00	-6.52		127.49
	+11.37	138.86	
18	12.		126.8
19	10.8		128.0
+68 $\frac{6}{\Delta}$	-4.23		134.63

2/19/13

Sherman
Keener

59

on Small Maple tree 150' S. of Sta 2+50

Peg near Sta. 4

on hub

on hub

on hub

Peg Near Sta 17+00

D³ Line

Levels

Transit on Page 19

		138.86	
20 + 00	6.1		132.7
TP Peg	-1.09		137.77
	+10.80	148.57 .6	
20 + 80	-5.9		142.7
TP Peg.	-0.12		148.45
	+12.73	161.18 .5	
21 + 00	10.8		150.4
+ 20	4.2		157.0
TP peg	-0.10		161.08
21 + 40	+13.70	174.78 .8	
	10.3		164.5
+ 55	3.2		171.6
21 + 69 $\frac{6}{\Delta}$	+ 0.7		175.48

2/19/13

Sherman
Keener

near Sta 21 + 00

Survey for change in
Location of Auburn Pk Blvd
and location of Elk Enclosure
N^3 Line on the flat Land

11+37 80 ⊙
= B. 15+41 5

6+84 3 ⊙

4+70 70 ⊙

3+24 70 ⊙

325

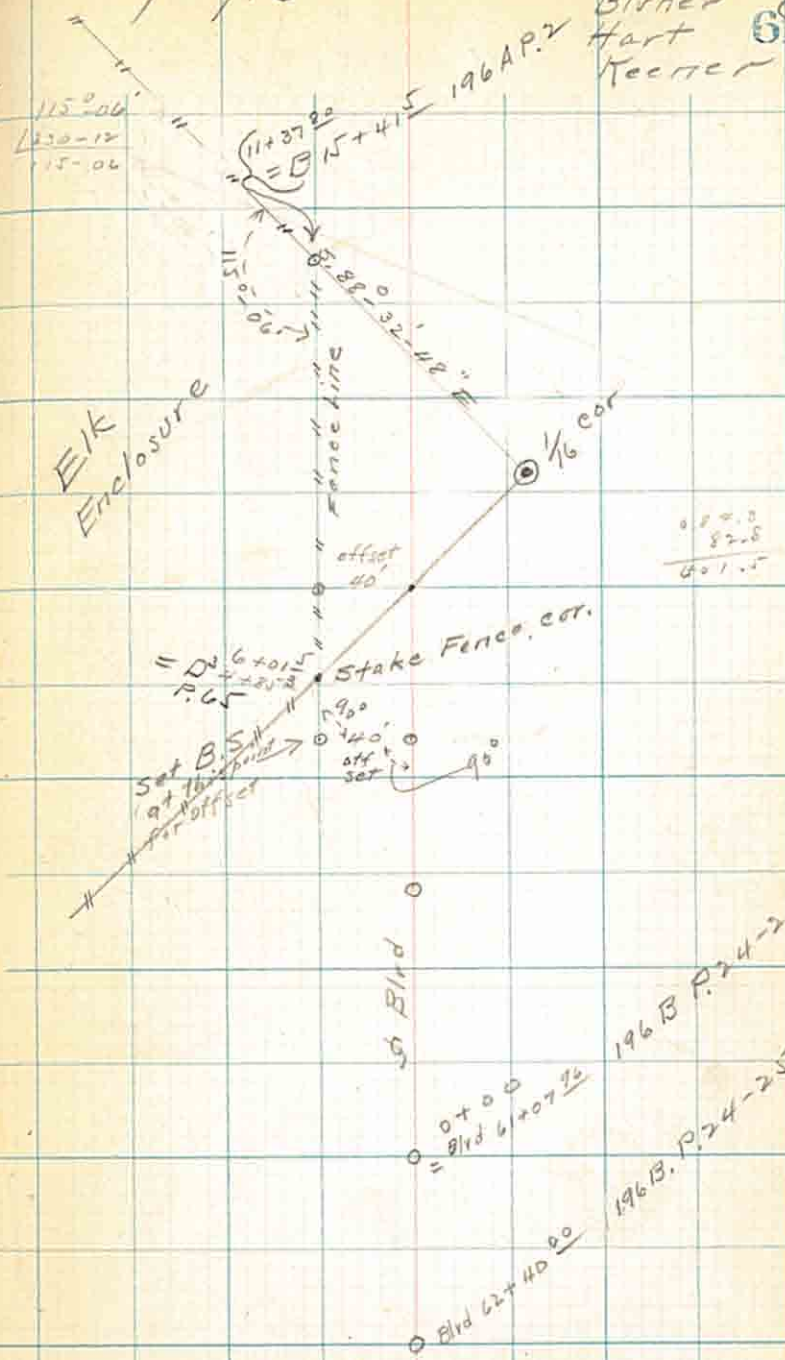
0+00 ⊙ S. 24° E

Blvd.
62+40 00 ⊙

1/20/13

Sherman
Blvher
Hart
Keener

61



H^3 Line

Location of Fence Line on E side Elk Corral on flat West of Bulk head.

5+41 $\frac{40}{\Delta}$

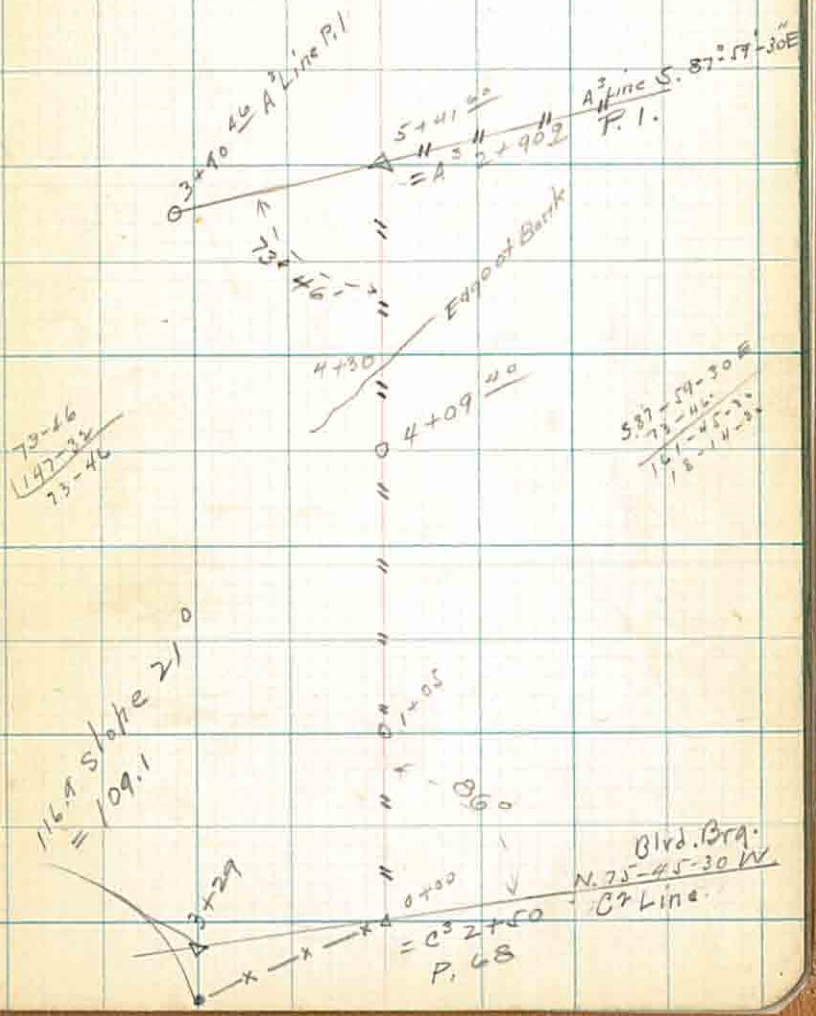
4+09 $\frac{40}{\odot}$

1+05 $\frac{40}{\odot}$

0+00 S. 18-14-30 W S 19° W

1/20/13

Sherman
Bluher
Hart
Keener



M. L. Right Bank White River
1867 By U.S. Govt.

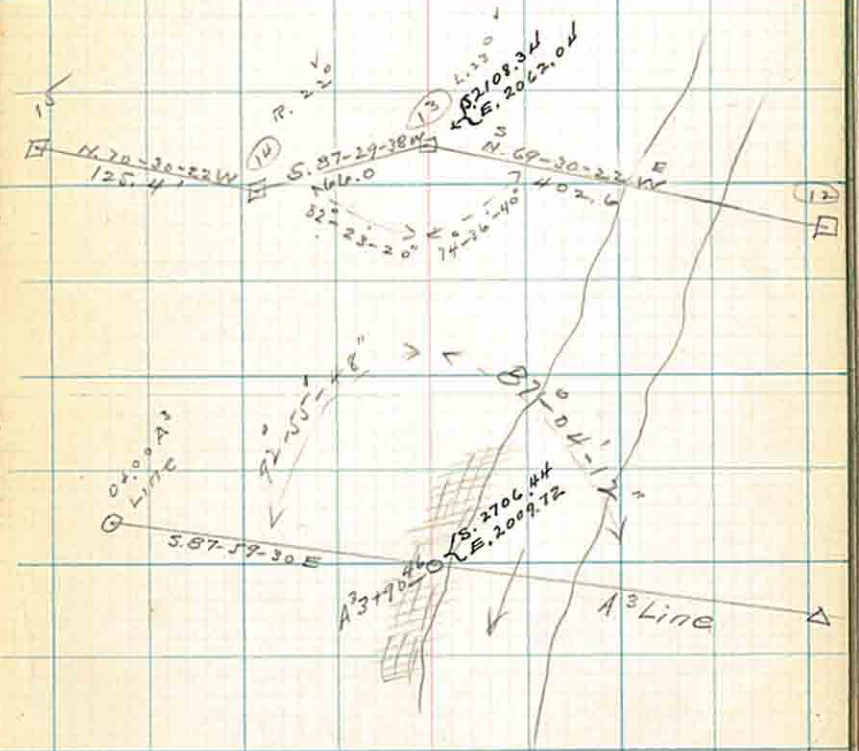
(13)

597.9

0+00 N. 5°-06'-18" E

2/18/13

Sherman
Keener



a^3 Line For Topography

16+55.2 △ L. 0°-35' S. 2°-02'-30" E.

13+29.90 △ L. 0°-28' S. 1°-27'-30" E S 1° E

346.10

9+83.80 △ L. 0°-10' S. 0°-59'-30" E S 30' E

312.10

6+71.70 △ L. 0°-57' S. 0°-49'-30" E S 0°-15' E

258.40

4+13.30 ⊙

413.30

0+00 △ S. 0°-34'-30" E
= A^3 24+00

28' L
2 | 56
28

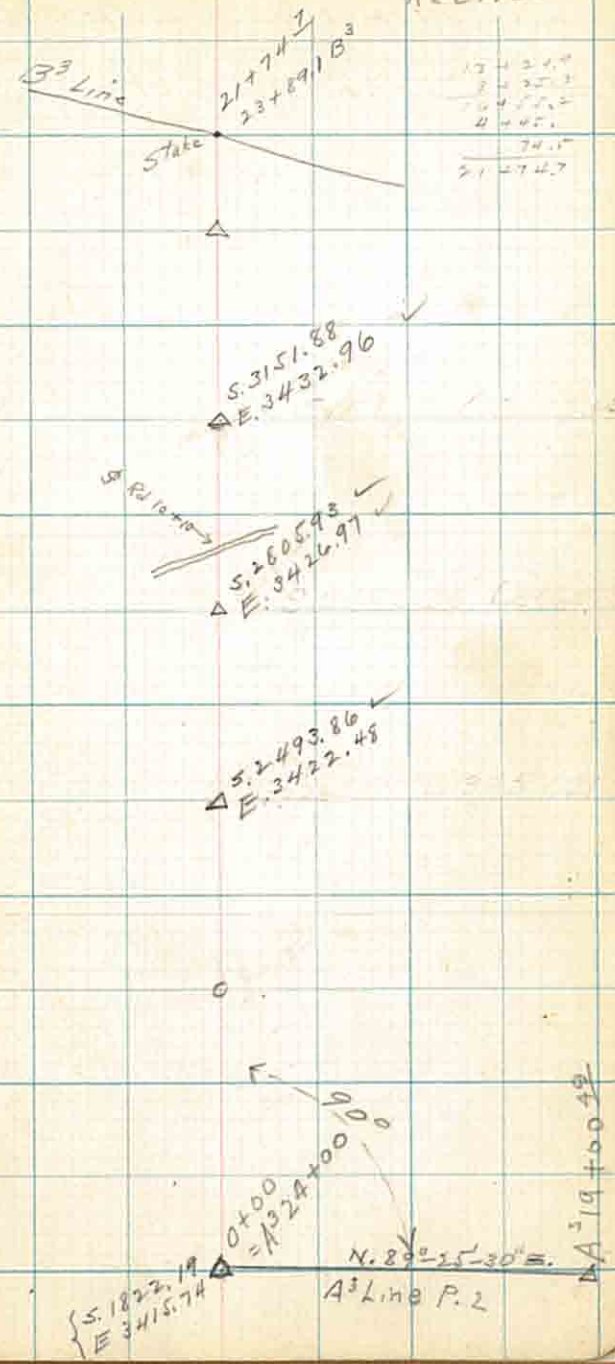
L. 0-10
2 | 20
10

L. 57'
2 | 1-54
0-57

1/9/13

Sherman
Graham
Hart
Keener

64



W. Line Elk Enclosure
Survey for fence Lines for
the Elk enclosure portion
M^3 Line of Lot 6 Sec. 29-21-5

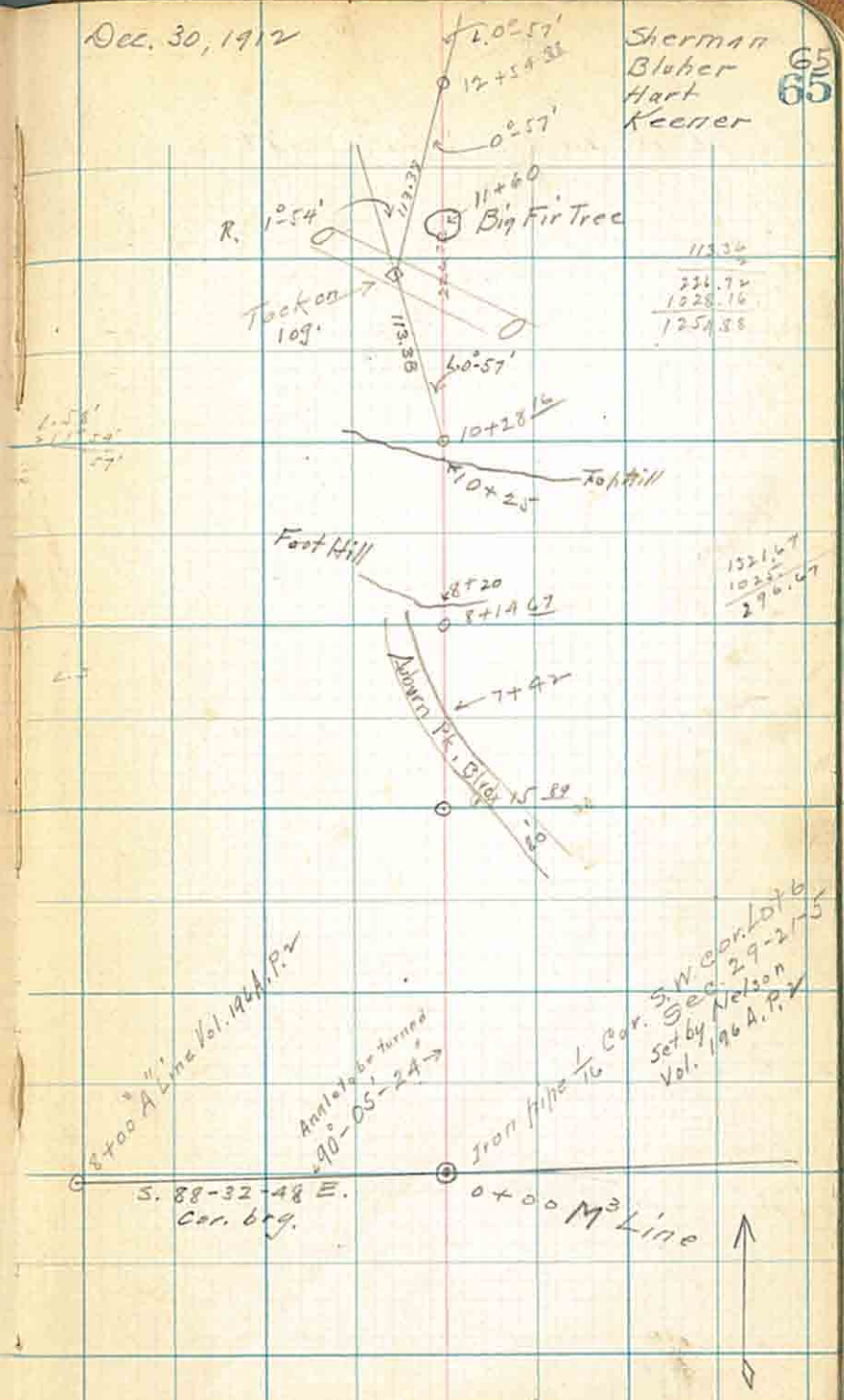
North on W. Line Lot 6 Sec. 29-21-5

12+54 88 △ L. 0°-57'
226.72 ← 113.38 △ R. 1°54'
113.38
10+28 16 △ L. 0°-57' N. 0-30' E
8+14 67 ⊙
6+15 89 ⊙
615.89
0+00 △ N. 1-32-36 E. N. 1°-30' E.
B. S. on
8+00 "A" Line
Vol. 196 A. P. 2

Dec. 30, 1912

Sherman
Bluher
Hart
Keener

65
65



W Line Elk Enclosure

M³ Line North on W. Line

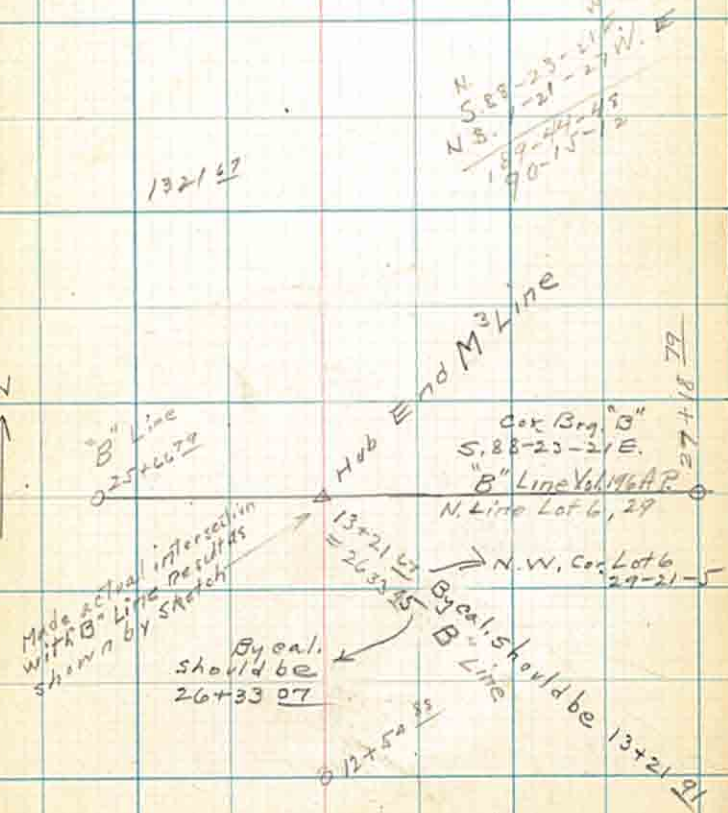
13+21 67/△ R. 90°-01' to Sta. 27+18 79 "B" Line Vol. 196 A.P. 2
= "B" 26+33 45

12+54 88/⊙ N. 1°-22'-36" E N 1°-30' E

Dec. 30, 1912.

Sherman
Keener
Bluher
Hart

66



S. Line Elk Enclosure
East Margin of Auburn Park
Boulevard bet. Sta. 50+64.73 and

Sta.	Angle	Dfls.	C. Course	M. Course
56+95.2	Intersect W. Line of Lot 6			
	B.S. on 54+57.2 R. 9°-32'			
+50				
	B.S. on 54+57.2 R 7°-45'			
56+00 Δ				
	R 5°-44'			
+50				
	R 3°-44'			
55+00				
P.C.	R 1°-44'			
54+56.71 Δ 8°-29'-35" C.R.				

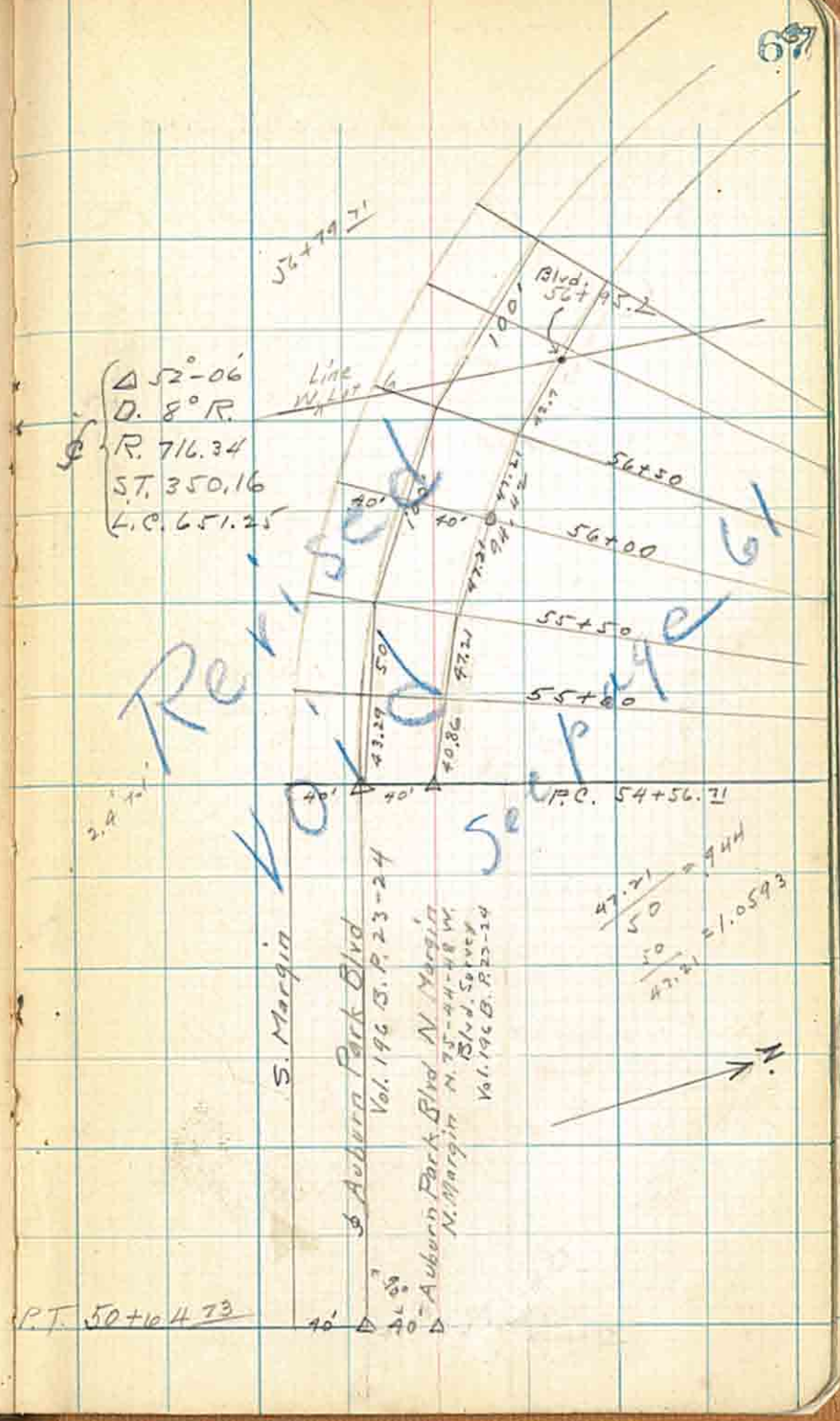
N. Margin
Δ 52°-06'
D. 8°-29'-35" R
R. 676.78
ST.
L.C.

2.54 - 1 ft.

391.98

N. 75°-44'-48" W N. W.

50+64.73 Δ P.T. AUBURN PARK BLVD.
Vol. 196 B. P. 23-24



Revised Void Sep 61

S. + E. Line of Elk Enclosure

C³ Line

12+49 91 ⊙ Iron pipe 1/16 cor. N.E. Cor. Enclosure

12+00 31 L. 34°-29'-30" N. 1°-13'-45" E N. 1° E

10+50 △ R. 7°-01' N. 35-43-15 E N. 36° E

8+87 50 △ L. 5°-00'-30" N. 28°-42'-15" E N. 30°-45' E

6+63 83 △ R. 11°54' N. 33°-42'-45" E N. 34°-15' E

6+31 58 ⊙ N. 22°-15' E

302.54

Slope Vert. Δ
336.32 + 25°-54'

3+29 04 △ L. 82°-15'-30" N. 21°-54'-45" E N. 22° E

329.04

C³ 0+00 ⊙ S. 75-44-48 E S. 75°-30' E
= P.T. 50+64 73 Blvd Brg.
Blvd. Vol. 196B P. 23

N. Line Lot 6.
B Line

L. 34-29-30

Iron pin

12+49 91

12+00 31

10+50

8+87 50

6+63 83

6+31 58

Stake Points bet 3+29 04 + 6+31 58

	Slope	Vert. Δ
Top of bank	116.9	21°
Slope	200	23°-21'
	300	26°

#3 42

#2 40

Edge Bluff

Top Bank

STAKE #1

82°-15'-30"

3+90 Foot of bank

3+29 04

Foot of Bank

2+20

Revised from Sta 0+60 to 2+50 see page 62

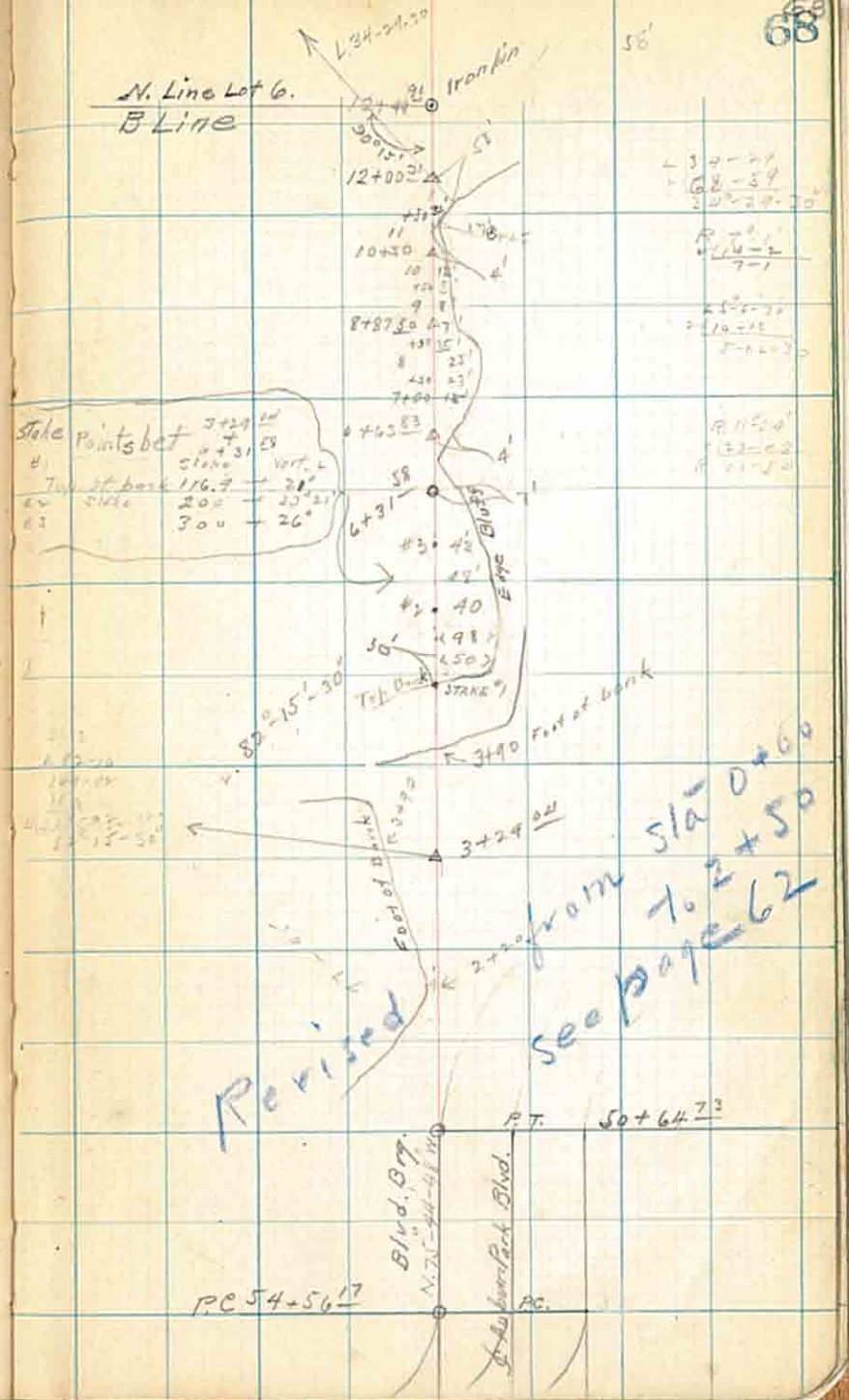
P.T. 50+64 73

Blvd. Brg. N. 75-44-48 W

Auburn Park Blvd.

P.C. 54+56 17

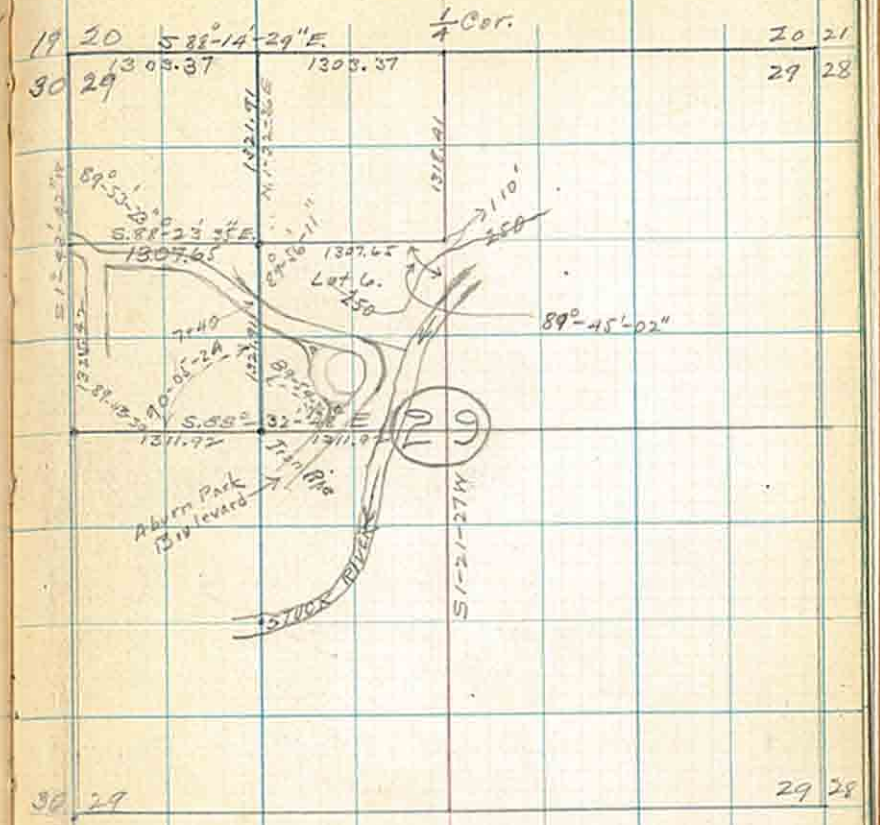
P.C.



Miscellaneous Notes.

From Sta. 50+64.73 P.T. Auburn Park Boulevard
to Sta. 54+56.17 P.C. brg. is N. 75°-44'-48" W.

SKETCH SEC. 29-21-5

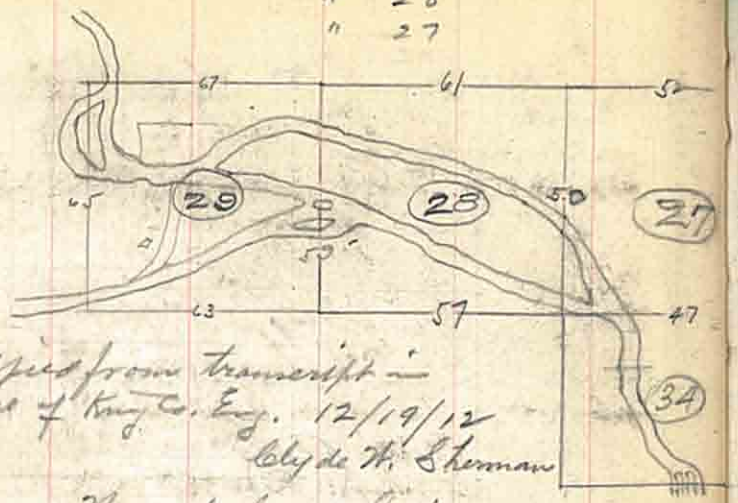


N. 88-23-35 W.
S. 1-21-27 W
89-45-02

90-05-24
N 88-32-48 W
1-32-36

1325.42
1307.65
2633.07

Cor. notes Sec. 29 - 21 - 5 T.N. R.E.
" 28
" 27



Copied from transcript in office of King Co. Eng. 12/19/12
Clyde W. Sherman

North bet. Secs. 28 + 29
Var. 21° E.

3.50 Descend
22.50 Top of White River bluff
27.00 Foot of Hill enter White river bottom
33.55 Slough runs W. water comes from White river.
33.80 N. bank of slough
39.27 Left bank of S channel of White river an alder 4 in dia for meander Cor. from which brs
An Alder 6 in dia brs. N. 35° W 5 lks
" " 3 in " " East 7 lks.
The point for the 1/4 post is in the river channel + cor not be established
41.00 Right bank of S. channel
42.20 Left bank of middle channel
To ascertain the distance across the river I sent axman

across to right bank of the middle channel
45.28 Right bank of the middle channel and on island.
48.06 A fir 20 in dia.
64.62 Left bank of N. channel of river crossed river and here on Rt bank
66.29 Set meander post from
A Maple 8 in dia. brs N. 83° E. 48 lks
A dead Cedar 30 " " N. 16° W. 38 lks
68.25 Slough course N. E.
69.00 Right bank
71.75 Creek 5 lks wide runs S. W.
72.50 Foot of bluff + leave bottom
76.40 Top of " brs. S. W. + N. E.
80.00 Set post for cor to Secs 20 - 21 - 28 + 29 from which
A fir 18 in dia brs. N. 12° E 63 lks
A cedar 12 " " S 42° E. 105 "
" fir 24 " " " S. 58° W. 156 "
No other tree convenient
Land on bluff 3" rate and broken

12/19/12 Sherman

31
7200
5280
1920

5280
2
10560
2640
13200
66

North bet Sec's 27 & 28
Var. 21° E.

5.20 A trail brs. E. & W.
6.20 An Alder 4 in dia & Left bank of White River, marked the alder for the Meander cor. from which
An alder 7 in dia brs. S 50 E. 12 lks.
A Balm 30 " " " S 47 W. 20 "
Island river filled with drift, & runs in several channels
11.60 To island and right bank of South channel of river
14.20 An Alder 10 in dia.
15.80 " " 24 " "
26.04 Left bank of N. channel of river Aug. 22, 1867.
Set witness post from which
An alder 4 in dia. br. N. 70 E. 11 lks.
" " 5 " " " S 65 W. 17 "
27.80 Right band N. channel and an alder 4 in dia marked the alder for Meander cor. from which
An alder 6 in dia brs. S 76° W. 7 lks
" " 5 " " " S 77 E. 5 "
30.70 Foot of bluff brs S.W.
38.00 Top " "
40.00 Set post 1/4 cor.

80.00 Post cor Sec. 27-28-33-34
A balm 24 in. dia brs. N. 47 W. 30 lks.
A V-Maple 4 " " " S 71° W. 10 "
A V-Maple 7 " " " N. 41° E. 35 "
A " " 3 " " " S 27 E 29 "
As the line bet 27-34 will strike the river
East on true line bet 27 & 34

5.71 Left bank of White river set meander post from which
An alder 8 in. dia. brs. S 40 W 14 lks
" " 12 " " " N 48 W 13 "

West on true line bet 34 & 27

12:00 Rd from Muckelshoot prairie to [illegible]
13:00 Descend
34.50 Top of bluff White river brs N.W.
40:00 Post 1/4 cor.
alder 12 in dia brs. N. 22 W. 62 lks.
fir 36 " " " S 54 W. 22 "
42.50 Foot of bluff enter White river bottom brs N. 60° E.
46.91 E. bank of slough or old river bed brs N 65° W.
47.46 Creek in bed of slough 20 lks wide N.W.
48.16 W. bank slough Aug. 19, 1867
51.00 Right bank White river
A cedar 14 in dia marked the cedar for meander cor. from which
A. Spruce 20 in dia brs. N. 12° E 13 lks
A. Maple 8 " " " S 87 E. 7 "

Part east River 51:00
" West " 5.71
" in River & Across 23.69
80.40

Mr. Sumgarth, Pierce Co. Belden Pacific

Walter Cole Treasurer office

Rd sup 3 yrs. ago 1/21/13

6.490
4.521
1.969

3.902
1.906
1.996
1.969
2 | 3.965
1.982 True Diff

.004 =
.013 =

143.41
4.72
148.13

		A³ Line	B³ Line	
A³ ✓	✓a³			
B³ ✓	✓b³			
C³ ✓	✓c³			
D³ ✓	✓d³			
E³ ✓	✓e³			
F³ ✓	✓f³	28+87	29+00	1935 ft. 5.1°-18'-08
G³ ✓	✓g	33+94.5	33+95	2035 "
H³ ✓	✓h³	40+03	38+75	2285
I³ ✓	i³	45+21	43+36	N. 1-21-45 E. 229
J³ ✓	j	24+00	North	
K³	k³ →	53+76 88/Δ	48+50	1570 ft.
L³	l³ →		52+91 5/Δ	1204
M³	m³ →		56+34 8/Δ	1145
	n³ →		60+94 8/Δ	896
	o³ →		66+27 5/Δ	600
	p³ →		71+35 2	

.78079
63.8
624632
234237
468474
49.814402

518.9
49.8
568.7

PROPERTY OF
KING COUNTY
ENGINEER'S OFFICE
905 COUNTY-CITY BLDG.
SEATTLE

PROPERTY OF
KING COUNTY
ENGINEER'S OFFICE
905 COUNTY-CITY BLDG.
SEATTLE